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Dear Nuts & Volts:

I just read the “Garage Parking Assistant” project by Dave Siegel in the December Nuts & Volts. While this solution sounds good, it does require a newer garage door opener with a light beam sensor.

My opener is of the older type without sensors and, some time ago, I came up with a “lower tech” solution that has been working fine for me.

The basis for my system utilizes the light circuit that is built into the opener’s motor box. I modified an inexpensive, hand-held laser pointer by bypassing the push-button switch so that it will always be on whenever power is applied. I then removed the batteries (two AAA cells, in my case) and permanently wired in a 3 volt DC wall wart power supply.

I mounted the modified laser and pointed it to an aluminum rod fastened to the opener motor box so that it pointed straight down. I then removed one of the two light bulbs in the opener motor box, screwed in a plug adapter, and plugged the wall wart into the adapter.

When the opener is activated, the remaining light bulb — and laser pointer — comes on and stays on for about two minutes. The laser pointer is aimed so that, when the red dot hits the middle of the dashboard, the car is in the proper position.

For any given system, it may be necessary to mount the laser pointer in a different manner and it will take a little trial and error to get it aimed to suit the driver.

Jerry Cobb
Oklahoma City, OK

Dear Nuts & Volts:

I have a comment regarding the November 2004 “Q&A” section called “Heart Rate Monitor.”

I, too, am on the lookout for an easy-to-implement way of recording a heart rate. Only, I’m interested in recording (or processing) the real ECG-signal. (The product T.J. Byers mentioned does not measure the ECG signal, but detects the pulse, which is not the same, technically.) So, I’m still interested in an ECG project.

Also I must strongly contradict T.J.’s view: Practically everything I could think of to build as a project can be bought for much less somewhere.

That’s our fate as hobbyists.

Christoph Klein
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Thankfully, most of my experiments since that fateful day have had better results and my dear mom smiles more than she fears for her first-born’s life. You’re probably wondering by now where in the world I’m going with this; well, let me tell you. As I’ve stated many times, I’m a very lucky guy: great job(s), a wonderful life, a wonderful family ... I really have no reason to complain, whatsoever. Part of my great job with Parallax is the myriad BASIC Stamp users I have contact with and, on many occasions, whom I get to assist. That is something I truly enjoy doing, but here’s the thing ... in our instant-gratification society, it seems like many BASIC Stamp users — especially those who are young and facing the deadline of school projects — are too willing to skip the experimentation part of the learning process. My friend and colleague, John Barrowman, calls this “the big bang technique.” They want it all at once: no reading of spec sheets, manuals, or experimenting with parts desired — just results, please. Right now!

To be candid, this is a little disappointing. Why? Well, those who “shotgun” their projects miss out on the sheer joy of experimenting and all the learning that comes with those experiments. It took Thomas Edison nearly 1,000 attempts to get a practical, working light bulb — and he was a heck of a lot smarter than most of us. Do you think the Wright Brothers looked up at a bird, and then headed for Kitty Hawk with a working version of the airplane? Of course not; there was a lot of incremental experimenting before they made a successful, powered flight.

With my exposure, I get bombarded with questions, some nearly as silly as “Jon, what would happen if I stuck my finger into a light socket?” My standard answer is “I don’t know — give it a try.” Okay, okay, I’m being a bit melodramatic (my other job is acting) to illustrate a point and, of course, I would never suggest that someone attempt something that would harm any person or BASIC Stamp module. I guess my point is that — for many of those questions — the answer would have been derived more quickly and with much deeper understanding through an experiment versus waiting for an Email from me.

I will quit preaching now ... but please let me beseech you — especially those who are young and just getting

For as long as I can remember, I’ve been interested in electricity and electronics. My first “way cool” experiment happened when I was in the second grade: I (correctly) deduced that a flashlight bulb would burn brighter if I connected wires to it and plugged them into a 120 VAC outlet. Yes indeed, I was correct — for about a millisecond before the bulb exploded. I’m not sure if it was the explosion of the bulb or the explosion of my mom (she has “pipes” when she needs them) that fascinated me, but I was forever fascinated.

Figure 1. ADC0831 Connections.

Figure 2. ADC0831 Timing Diagram.
started — to experiment. It’s fun; it’s a lot of fun. And I promise that you won’t soon forget what you learn from your experiments — especially those experiments with unexpected results.

**Analog Fun**

Okay, let’s experiment. For reasons I can’t explain, a bunch of customers seem to have come up with the ADC0832 (two-channel ADC) and are wondering why the application code for the ADC0831 floating around doesn’t work with it. (That sound you just heard was the old-timers smacking themselves on the forehead and exclaiming, “Duh!”) The reason, of course, is that the ADC0832 is NOT the same as the ADC0831. It’s in the same family, yes, but it is not the same part, so it will require different connections and code.

For our experiments this month, we will need just a few parts: the ADC0831 and ADC0832 (or ADC08832) that we just mentioned, a couple of 10K trim pots, and a project board to connect things to the BASIC Stamp. You can use anything handy: the BOE, the NX-1000, or — my new favorite — the Parallax Professional Development Board.

Let’s start with the ADC0831. I will admit that I’ve kind of glossed over the details of this part in the few projects where I used it, because I (incorrectly) assumed that it — and code for it — had been around for such a long time that everyone who used the BASIC Stamp had an understanding of how the ADC0831 works and how to apply it. As is occasionally the case … I was wrong.

Grab your parts and connect the circuit shown in Figure 1. For the time being, make sure that you have the pot connected to Vref moved to the +5 V position (confirm with a multimeter). Before we get on to the code, let’s have a look at a couple of technical details that the manufacturer provides in the form of a timing diagram. The timing diagram shows the signals in and out of a device and the relationships vis-à-vis time. Figure 2 shows the essential signal timing for the ADC0831.

What this diagram shows us is that we must take the CS (chip select line) low to initiate a read of the ADC0831. Why? Well, maybe we can’t find an ADC0832 and we need two distinct channels. By using separate CS lines to control each device, two ADC0831s can share the Clock (CLK) and Data Out (DO) lines. After the CS line is brought low, the CLK line needs to be pulsed activate the device. After that, eight additional clock pulses cause the data bits to be shifted out of the ADC0831.

At first, we may be inclined to write a subroutine that looks like this:

```basic
Read_0831:
    LOW CS
    PULSOUT Clk, 50
    SHIF Tin Dio, Clk, MSBPOST, [adc\8]
    HIGH CS
    RETURN
```

It all makes sense, right? We bring the CS line low, blip the clock line with a pulse to wake the ADC0831, shift eight bits in, and then finish up by returning the CS line high. Anything wrong with that? Nope, not a thing. Can the routine be improved? You bet.

Through understanding and experimenting (there’s that dreaded “e” word ...), we find that we can remove the **PULSOUT** instruction and shorten the code to look like this:

```basic
Read_0831:
    LOW CS
    SHIF Tin Dio, Clk, MSBPOST, [adc\9]
    HIGH CS
    RETURN
```

The first question that probably comes to mind is “How can you use nine clock pulses with an eight-bit value?” We can do that by understanding what happens to a value when we use **SHIF Tin**. Let’s get gory with details, shall we?

When using MSB mode, the target variable is shifted left (MSB goes into la-la-land and a 0 is placed in Bit0), then the data line is sampled (in this case, after the clock-POST mode because the ADC0831 makes data bits available after the clock pulse falls), and that bit is placed into the Bit0 of our target variable. When we get to that ninth clock, the first bit sampled gets shifted from the MSB (Bit7, in this...
case) into the great bit-bucket and is discarded. Here’s how we could simulate the SHIFTIN using a loop:

Shift_In_MSBPOST:
FOR idx = 1 TO 8
    adc = adc << 1
    PULSOUT CLK, 50
    target.Bit0 = Dio
NEXT

For obvious reasons, using SHIFTIN is easier, but understanding the mechanics is helpful when we want to optimize code, or — if needed — port to a lower-featured controller like the BS1. Now that we can read the ADC0831, it's a fairly simple matter to display the data:

Main:
DO
    GOSUB Read_0831
    mVolts = adc */ Raw2mV
    DEBUG CRSRXY, 10, 2, DEC3 adc,
    CRSRXY, 10, 3, DEC mVolts DIG 3, ".", DEC3 mVolts
LOOP
END

This code uses a constant called Raw2mV that is used to convert the input voltage to millivolts — just keep in mind that the value in the program is for +5 on Vref. The value of Raw2mV is $139B, which is the equivalent of 19.6 when using the */ (star-slash) operator. Remember that star-slash multiplies by units of 1/256, so it’s a convenient way to multiply fractional values. How’d we get $139B? First, we take the Vref voltage of 5.00 and divide it by 255, which is the maximum output value from the ADC0831. This gives us 0.019607. If we multiplied directly by 0.019607, we would end up with very small output values, so what we’ll do is multiply by 1,000, which will cause the result of our multiplication to be millivolts (1/1,000 of a volt). Now, we take 19.607 and multiply that by 256 for the star-slash operator. We get 5,019. My habit is to convert to hex — $139B — as this puts the whole portion of the value in the high-byte
and the fractional portion of the value in the low-byte.

After calculating the millivolts value, the display is handled with `DEBUG` and a couple of neat tricks using the `DIG` operator and the `DEC` modifier (see Figure 3). If you don’t fully understand what’s happening with the output, here’s your big chance: open the help file and read up on `DEBUG`, `DIG` (in the operators section), and using formatters (like `DEC`). Then ... you got it ... experiment. A few minutes spent experimenting will save you hours of frustration later.

Once you have the display figured out, it’s time to play with the Vref voltage and examine its effect on the output data. Using your multimeter, you should be able to prove the following behavior of the ADC0831:

\[ \text{counts} = \left( \frac{\text{Vin}}{\text{Vref}} \right) \times 255 \]

What you’ll also see is that the output hits a ceiling of 255 when Vin exceeds Vref; we need to keep this in mind with designs when Vin could exceed Vref. One last thing before moving on — and, again, you’re on your own after I give you a little push. The ADC0831 is typically used as a single-ended device, but can also be used in differential mode. The Vin discussed above is really the difference between Vin(+) and Vin(-). Let’s say we had an application where we wanted to know how much greater one voltage is than another. We can do it with the ADC0831 by connecting the greater voltage to Vin(+) and the lesser voltage to Vin(-). The output will be the difference between the two values, relative to Vref. What happens if Vin(+) goes lower than Vin(-)? I know — because I did an experiment to find out. It’s your turn ...

Two for the Price of One

Okay, let’s give the ADC0832 (or ADC08832) a try, shall we? I think part of the problem some users have had with this chip is that it comes in the same physical format as the ADC0831 (eight-pin DIP). However, the connections aren’t the same and neither is the code (it’s close, though).

Connect the circuit shown in Figure 4. Immediately, you’ll notice a couple of things: the ADC0832 has a DI (Data In) line and there is no Vref pin (Vref is tied internally to Vcc). One of the nice things about using the BASIC Stamp is that it can change an I/O pin’s state on the fly, so we don’t need separate lines for DI and DO — we can tie them together. We don’t want to connect them directly to the BASIC Stamp. Why? Well, as you’ll see in just a moment, the DI line is expecting three control bits after the CS line falls; then, it activates the DO line and starts pumping out data. If we made a programming error that caused `SHIFTOUT` to send more bits than required, we could end up with a data collision. Worse, one side could be high while the other is low, causing a direct short and perhaps doing damage to the ADC0832, the BASIC Stamp, or both. A $0.05 resistor is cheap insurance; it will protect us from a problem and has no ill effect on communication between the BASIC Stamp and the ADC0832.

Figure 5 shows the ADC0832 interface timing. As with
the ADC0831, we start by taking the CS line low. This time, though, the start bit is output (by the Stamp) on the Dio line and must be a 1. The next two bits configure the ADC0832. The first of those two bits sets single-ended or differential mode. The final bit serves as the channel indicator when in single-ended mode or sets which input is positive when using differential mode.

Let’s code it up:

```assembly
Read_0832:
  LOW CS
  SHIFTOUT Dio, Clk, MSBFIRST, [\%1\1, sglDif\1, oddSign\1]
  SHIF Tin Dio, Clk, MSBPOST, [adc(oddSign)\8]
  HIGH CS
  RETURN
```

Once again, the code matches the timing diagram without a lot of mystery. After taking the CS line low, we have to shift out a “1” to get things started. Since we only want to send a single bit, the \%1 parameter is used with the value. Next comes the mode bit: 1 indicates single-ended and 0 indicates differential. Finally, we shift out a bit that indicates the channel for single-ended mode or the positive (+) channel for differential mode. When the data is shifted in, we place it into the selected element of a two-byte array.

The neat thing about the ADC0832 and the circuit we put together is that we can try its various modes without changing any wires. While the demo for this device is a little more involved than with the ADC0831, it’s really no more complicated:

```assembly
Main:
  DO
    sglDif = Sgl
    FOR oddSign = 0 TO 1
      GOSUB Read_0832
      mVolts(oddSign) = adc(oddSign) */ Raw2mV
      DEBUG CRSXY, 7, (4 + oddSign), DEC3 adc(oddSign), TAB, DIG 3, ",.0", DEC3 mVolts(oddSign)
    NEXT
  sglDif = Dif
  FOR oddSign = 0 TO 1
    GOSUB Read_0832
    mVolts(oddSign) = adc(oddSign) */ Raw2mV
    DEBUG CRSXY, 7, (9 + oddSign), DEC3 adc(oddSign), TAB, DIG 3, ",.0", DEC3 mVolts(oddSign)
  NEXT
  LOOP
```
The program simply loops through both channels in each of the two operating modes, displaying the raw counts and calculated voltage output as before. Figure 6 shows the results. If you look very closely at that display, you’ll notice that the differential mode differs from the single-ended mode by about two counts — this had to do with a noisy test set-up and I could never really get a single-ended reading to hard zero. Finally, Figure 7 shows you the result of an experiment of mine with the ADC0832 set-up. I recently purchased a digital scope/logic analyzer and I hadn’t had a chance to use the logic analyzer portion of it. So, I connected three probes (one each for CS, Clk, and Dio) and captured a part of the transmission that corresponds to the values in Figure 6.

What’s interesting to note is the spacing between the configuration bits versus the data bits. Why do you suppose this is? If you go back and look at the subroutine, you will see this line:

```
SHIFTOUT Dio, Clk, MSBFIRST, [%1\1, sglDif\1, oddSign\1]
```

This is actually quite complicated. We’re asking the BASIC Stamp to send one bit of a constant value, then go retrieve a variable and send one bit from it, then go get another bit and send a single bit from it. This explains the wider timing between the clock pulses going out versus the pulses for the data coming in (which only has to deal with a single variable).

I’m leaving it up to you now — go forth and EXPERIMENT! Remember that Rome wasn’t built in a day and neither will all of your projects. What you’ll find is that — after you’ve experimented for a while — your internal knowledge base will grow to the point where projects will come faster. That said, don’t be afraid to try little things, as lots of little things add up to greatness.

Allow me to wish you and your sweetie a Happy Valentine’s Day. (Guys, robots do NOT make cool gifts — unless your girlfriend is an engineer or reads *Nuts & Volts* and *SERVO Magazine*. Remember, chocolate still works.) And, until next time, Happy Stamping.  

---

**Figure 5. ADC0832 Timing Diagram.**

**Figure 6. ADC08x32 Output.**

**Figure 7. ADC08x32 Scope Capture.**

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Another Step Toward Fusion

For decades, we have gazed hopefully at the prospect of practical nuclear fusion and the promise of cheap, safe, non-polluting energy. The dream has remained elusive, but progress is, in fact, continuing. The next step may consist of the National Compact Stellarator Experiment (NCSX), now under construction at the Princeton Plasma Physics Laboratory (www.pppl.gov).

To produce useful amounts of energy from fusion on Earth, you need to produce a plasma with the required temperature, density, and heat retention. To achieve that, you must determine the best shape for the hot, reacting plasma and the magnetic fields that keep it in place. Advances in magnetic confinement physics and computational capabilities have yielded a new configuration — the compact Stellarator, which is somewhat more complicated and presumably more efficient than existing tokamak devices (primitive fusion generators). The NCSX vacuum vessel, now under construction, is described as resembling a twisted doughnut. It will be made of Inconel 625 and be press formed with 0.375” walls.

According to PPPL, the device’s modular coils are among the most complex, innovative electromagnets ever designed, employing 18 winding forms that consist of non-magnetic stainless steel castings with the winding surfaces machined to a tolerance of plus or minus 0.020”. The largest will be 110” tall and each will weigh approximately three tons. The winding forms will provide the backbone of the modular coil system and will be strong enough to support electromagnetic loads in the range of 7,000 pounds per inch. The $86.3 million project is scheduled to begin operation in 2008.

Microengines Power Small Devices

On a much smaller level — but perhaps closer to commercial application — is a new microgenerator developed at Georgia Tech (www.gatech.edu) aimed at providing power to small electronic devices, such as cell phones and laptops. The 10 mm wide microgenerator produces useful amounts of electricity by spinning a small magnet at 100,000 RPM above a mesh of coils manufactured on a chip, producing about 1.1 W of power.

When coupled with a similarly sized, gas-fueled microturbine (or jet engine), the system — called a “microengine” — is said to have the potential to deliver more energy and last 10 times longer than a conventional battery. In the lab, the Georgia Tech team used an air-powered drill (similar to what your dentist uses to torture you) to simulate the spinning of the magnet by the microturbine (still under development at MIT). Now that initial tests have been successful, they hope to increase the speeds to squeeze out more power.

One of the team’s key problems was figuring out how to spin the magnet fast enough to get useful amounts of power while keeping the magnet from breaking apart; high performance magnets are brittle and can be disintegrated by centrifugal force at high speeds. To overcome this problem, the researchers optimized the magnet’s dimensions and encased it in a titanium alloy. The goal is to eventually increase the output to as much as 20 to 50 W, allowing it to replace batteries in a range of electronic devices.

Computers and Networking

“Pocketable” PC

In line with the never-ending evolution toward devices that are too small to be used by human fingers, Sony has introduced the VAIO U-Series “pocketable” PCs. The 1 lb device doubles as a media player and...
includes integrated 802.11b/g wireless LAN capability. You can enter text using a stylus and virtual keyboard on the unit’s tough panel screen or you can plug in the fold-out keyboard (included) if you have room.

Other features include a 5” display, Memory Stick® and Compact Flash media slots, and thumb controls for changing display orientation. It is powered by a Pentium® M processor and Windows® XP Professional OS and you even get a mobile AC adaptor, headphones, and a VGA/Ethernet adapter. The port replicator allows the batteries to be charged and permits the connection of peripherals, such as a mouse, hard drive, or external display. The bad news is that it will set you back about $2,000.00. For more details, visit www.sonystyle.com

New Browser in Town

Late last year, the Mozilla Foundation released its web and Email applications suite, based on the original open source Netscape Communicator product (which was originally named Mozilla). The suite consists of the Firefox 1.0 web browser and the Thunderbird 0.9 Email client. (As of this writing, Thunderbird 1.0 was available, but not officially in final release.) It appears that Firefox is an unprecedented success, with nearly 5 million copies downloaded in the first couple of weeks after its release. According to W3Schools (www.w3schools.com), Firefox had already gobbled up nearly 20 percent of the market by December 2004, second only to Internet Explorer 6, which had 68 percent.

The suite, which has scored highly positive reviews, is available in 26 languages for Windows, Mac OS X, and Linux and can be downloaded from www.mozilla.org/products/firefox/all.html Other products are available or under development, including Bugzilla (a bug tracking system), Camino (a web browser optimized for Mac OS X with a Cocoa user interface and the Gecko layout engine), and Calendar Project (a cross-platform calendar application).

“World Community Grid” Launched

Would you like to help conduct research to unlock the genetic codes that underlie diseases like AIDS and HIV, Alzheimer’s, and cancer? Improve forecasting of natural disasters? Support studies that can protect the world’s food and water supplies? Resolve other dreadful human afflictions? What if it didn’t require any effort, re-education, or significant expense on your part? Well, step right up. You can start now.

IBM (www.ibm.com) — along with representatives of many scientific, educational, and philanthropic organizations — recently launched World Community Grid (WCG), a global humanitarian effort created to apply the unused computing power of individual and business computers to help address the world’s most difficult health and societal problems.

To participate, all you have to do is download a small program — about the equivalent of a screen saver — that links it to the WCG. When idle, your computer will download data on a specific project from WCG’s server, perform computations on the data, send the results back to the server, and ask the server for a new piece of work.

Each computation that your computer performs will provide scientists with information that accelerates the pace of research. You can even track your participation and monitor how many computational contributions you have made.

The software runs only while your PC is operating, so there is no need to keep the machine powered up for extended periods. As of this writing, the WCG had 26,644 members providing time on 35,057 computers and the numbers are growing constantly. If your machine runs Windows XP, 2000, ME, or 98, you can volunteer by downloading the free software and registering at www.worldcommunitygrid.org

Circuits and Devices

Active Ethernet Simplifies Installation

The power-over-ethernet (PoE) concept, a.k.a. “active Ethernet,” eliminates the need to run 110/220 VAC power to wireless access points and other devices on a hardwired local area network. This increases installation flexibility and can reduce installation costs. All you need to
set it up is an “injector” that inserts a DC voltage onto a run of CAT5 cable and a PoE-compatible device at the other end. Alternatively, you can attach a “picker” or “tap” to a non-PoE-compatible device and achieve the same effect. The concept is complicated somewhat by the need to determine whether you need a passive or regulated tap, but it’s not brain surgery.

Hyperlink’s model PS4820-PoE provides this capability, allowing you to connect to wireless LAN access points and bridges, WiFi amplifiers and amplified antennas, voice over Internet Protocol telephones, web cameras, Bluetooth® access points, and other devices. The PoE injector and 48 VDC, 20 W power supply are provided in one unit and it operates from a 100-200 VAC input. It is compatible with most wireless LAN standards, including 802.11a, 802.11b, 802.11g, and Bluetooth, as well as GSM, ISM, UNII, WiFi, PCS, and RFID applications. Single units are priced at $39.95, with quantity discounts available. Details are available at www.hyperlinktech.com

Better Bass From Tubular Speakers

Whether your goal is to enjoy more accurate sound reproduction from your home stereo system or pound your brain into a tapioca consistency while driving around in your chopped, channeled, louvered, and lowered Kia, it would be nice to avoid sacrificing inordinate amounts of space to huge subwoofers. The linear array transducer (LAT) technology from Tymphany Corp. (www.tymphany.com), is designed to achieve that. According to the company, the device, “infuses the low frequency response of a subwoofer into a full range woofer with a highly efficient and novel tubular form factor. The Tymphany LAT makes it possible to achieve lower frequencies from today’s space-sensitive products and to develop more highly integrated consumer and professional audio products in the future.”

In a departure from conventional cone loudspeakers that displace air across a single diaphragm, the LAT technology displaces air using a linear array of multiple smaller diaphragms to generate sound at high decibel levels across a range of frequencies from 20 Hz to above 4 kHz. Sound radiates through multiple flow ports along the side of the housing, producing deep bass using one-third of the space of a traditional cone transducer. The technology employs a balanced drive design that consists of a series of coupled diaphragms that are driven by opposing end motors. One motor drives half of the diaphragms while the other motor drives the other half in opposition. The use of opposing end motors is designed to cancel out structural vibration, so the transducer will not shake or transmit structure-born vibrations to critical circuitry.

The technology is scalable from 2” to 12” in diameter at virtually any length. As of this writing, no information was offered as to commercially available equipment, but the patented design is expected to appear in audio products soon.

Industry and the Profession

PC Company Deaths Predicted

According to the research and analysis company Gartner, Inc. (www.gartner.com), three of the top 10 PC manufacturers will bite the dust by 2007. The company forecasts that annual revenue growth for PC makers will average only two percent from 2006 through 2008, which will force the marginal companies out of the market.

At present, the top 10 consists of (in order of units shipped) Dell, HP, IBM, Fujitsu Siemens, Toshiba, Acer, NEC, Legend, Gateway, and Apple Computer. Shortly after Gartner’s announcement, several news articles revealed that IBM put its PC business up for sale, with a Chinese company as a likely prospective buyer. However, it is expected that the company will continue to sell IBM-branded products, even if they are built by someone else.

Which companies will disappear? Time will tell.

Free Tutorial Previews Available

The IEEE Communications Society is offering free five minute previews of its enhanced conference tutorials online. Topics available for preview include security and information assurance, smart antennas for wireless systems, an introduction to universal plug and play (UPnP), and broadband wireless IP.

Originally presented at recent IEEE Communications Society sponsored conferences, the tutorials run 2.5 to 5 hours in length and contain the original visuals and audio. They are available for purchase for $200.00 for society members and $250.00 for non-members. For more information, visit the society at www.comsoc.org NV
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Circle #52 on the Reader Service Card.
As we approach middle age, we often try to re-assert our youth. For some, this manifests itself as an overwhelming need to buy a red Corvette, sunglasses, and possibly trade in the old wife for one with that “new wife smell.” For geeks like me, we remember the old days when a computer was powerful if it had a video screen, mass storage was something you did with an audio cassette, and Basic was this remarkable language that allowed you to make your computer do amazing feats of magic by drawing different ASCII characters on your screen.

You may remember back to your first Basic program. It probably read something like this:

```
FOR A=100 TO 0 STEP-1
PRINT A;
PRINT " bottles of beer on the wall"
NEXT A
```

It was interpreted Basic and it ran painfully slow if you did anything iterative, but — back then — you saw yourself as an unstoppable god with this new power. I recently found myself looking for that power and simplicity in a PC-based language. My goal here is to eventually simulate and then finally interface to robots with a relatively easy-to-use and inexpensive language. I could then share my source code with you and not break your bank accounts. I decided on looking into five different Basic implementations — each with its own strengths and weaknesses:

- **Xbasic** Free
- **RealBasic** $149.00+
- **BlitzBasic** $100.00
- **DarkBasic** $49.00
- **PowerBasic** $199.00+

I intentionally omitted Visual Basic.net out of pure prejudice against Microsoft’s monopoly on the computer market, though I am sure I will regret it.

Now, I know there are other Basic implementations out there, but I decided to limit the scope of my investigations to the ones that seemed to have the highest promise to do all the things that I needed them to do. My needs seem modest enough; I just want to incorporate mathematics, graphics, communications, and ease-of-use into my projects.

Mathematics is important to me because I rely on trig functions a lot. I like to simulate my mathematics in Excel, for instance, but — when you start building spreadsheets that make your workmates worry for your sanity — you have to examine what and how you do your simulations.

Having been an art major in college, I am a very visual person. I really consider graphics as the force that got me into computers to begin with. I use graphics to represent complex mathematical concepts and mechanical interactions; I make it a point to really thrash away at my spreadsheets to make them draw pretty diagrams via graphs and charts.

The communications are important to me because, one day, I hope to transfer the data my software generates into data living within an actual hardware representation of the thing I am simulating. I hope to do genetic algorithms and artificial neural networks, but these are often too time-consuming to let take place in real time.

Ease-of-use ... what can I say, I remember when Basic was just that. After all, for those of you not in the know, Basic stands for Beginners’ All purpose, Symbolic Instruction Code. You would think it would be easy, but now I can assure you that this is not always the case.

To me, the one thing that truly isolates me from true simplicity is the IDE (Integrated Development Enterprise) itself. It used to be a convenient means to do some simple things with a compiler, a level of isolation from the nitty-gritty of the software’s core. Now it seems to me that, in some instances, it has gone too far.

**BlitzBasic3D**

BlitzBasic3D — or B3D — is, in essence, a Basic wrapper on the really powerful DirectX 3-D wrapper for the really, really powerful commands internal to your graphics card. On top of this are a lot of sound, sprite, file, network, and math commands. Most of everything I could ever want in graphics is here: two- and three-dimensional graphics commands, trig, entity collision, and textures. The one lacking piece was the ability to use the COM ports easily. There are third party extensions available (called DLLs for Dynamically Linked Libraries), but I was not able to get them to function on my machine. I did get the parallel port communications working, however.

As discouraging as the lack of COM ports is, getting graphics out of this is frightfully easy. The IDE does not obfuscate or isolate; it is simply a useful tool. I did, however, make the
unfortunate mistake of buying it from a site other than BlitzBasic.com and, as a result, waited many moons for my registration number. I purchased from BlitzCoder.com and, eventually, they locked my thread on their forum complaining about the poor response time I was getting from them. Remember, BlitzBasic or Blitz Research is good; BlitzCoder is bad.

I really want the COM port to work and intend to stay tuned to see what comes of it. Overall, it’s really cool and fun; I will try to get the data I need through the TCP/IP functionality before I give up.

**DarkBasic**

DarkBasic is everything B3D is, but a little more — more graphics functions, faster, cooler, slicker. It’s a little more complicated than B3D, but the power is worth it. The pro version comes with a lot of neat stuff, like 3-D models. What was fun here is how easy it is to get stuff that looked so cool up and running so quickly. I built an MP3 player in two hours, for example.

Again, I failed at my mission objective. I have not succeeded at getting DBP to access the COM ports via a DLL. I only mention B3D and DBP because I have to believe that, one day, they will make COM ports standard or one day some individual will be able to make the external DLL that allows the COM ports to operate and all my troubles will be solved. I have a friend who is supposed to help me out on this one, possibly just writing the DLL I need from scratch.

**Xbasic**

Okay, down to the point. There’s no direct method for COM port access, except through the Windows API (Application Program Interface). Avoiding the API is the whole reason I was going down this road to begin with. Top it off with a lot of libraries for everything and it starts getting complex.

It appears to be very powerful and fast; I imagine that, with enough dedication, I could get it to do what I want, but I am really diverting from my course at this point. I am starting to grit my teeth at night over this and that is just not healthy. The COM port thing has got me bugged.

I downloaded Xbasic from www.maxreason.com/software/xbasic/xbasic.html It is worth a free download and people out there have succeeded in getting the COM ports to work.

**RealBasic**

RealBasic is a fun one. I did manage to get the COM port talking to a microcontroller very quickly, but the whole methodology is alien to me.
RealBasic is an event-driven Basic: sit around, wait for something to happen, and respond. I still haven’t gotten used to that way of doing things. The development environment is a bunch of objects like buttons, windows, or deeper level items that you drag to your main window. You rename them intelligently and stick in bits of code that are associated with the actions you care about. It’s truly the epitome of OO (Object Oriented) programming and I loathe it.

RealBasic does everything I need it to, is inexpensive, and has the math support I need. An added bonus is that you can compile for the Mac, as well. I really have to apply myself to this one because it does everything I need, but I am a stodgy old man — resistant to change, set in my ways, and more apt to be hosing down kids who wander onto my property looking for lost baseballs than changing the fundamental way I code.

PowerBasic

PowerBasic promises access to the COM ports without any calls to the Windows API, which is something that only RealBasic has been able to do. Unfortunately, PowerBasic doesn’t directly support graphics, but it does allow you to access the API without having to use a DLL. In addition, there is also an external, third party graphics API wrapper available.

Now, while this seems like just another trade-off, there is an advantage to buying the graphics support; you get the quality of someone’s efforts to produce a final product, not someone else’s hobby in the form of a DLL. Simply put, being able to use the API strips off a layer of complexity because you do not have to rely on external DLLs. In addition, because you access the API directly, you can wrap your own DLLs, too. This is a nice way to compliment other languages that can make use of them.

Another nice feature of PowerBasic is that it is really, really fast. For some simulations and neural networks, you can’t beat speed. I haven’t done a direct comparison, but — for the serious stuff — PowerBasic is the winner. NV


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Made by Johnson Electric 12 VDC @0.85 A no load, 17,000 rpm, 3 vdc @ .3 amps 4,200 rpm, 6 vdc @ .3 amps 8,500 rpm. Similar to Johnson Electric HC313MG series but higher power. Actually runs as low as 1 volt op peration (1000 rpm, .46 amps). Size: 2” x 1.5” dia 7/8” long eccentric brass shaft end easily broken off to form a .5” long x .312 dia round shaft end. 0123850R C size Sub C Quality from our factory buyout. Big voters will love the 2,000 LED boxes! These LEDs are the smaller T1 size with full leads, available in Red or Green. Imagine 2,000 LEDs for less than a penny each! 0131258R High Bright 500 pc box $15.00 0131259R Standard Bright 500 pc box $15.00 0130965R Box of LEDs Red 2000pcs $19.95 0130966R Box of LEDs Green 2000pcs $19.95

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Wow! What a cool item! Brand new laser scanner module (size 1x1x.75”) includes red laser, beam splitting mirror, opamps, photo sensor, transistors, processor, ICs, etc. From handheld laser barcode reader. We sold out of the last style we had! No specs, but buyers figured out the hook up for the laser gun. We’ll post on the web any new info on this one, should be easy, has just 12 pins on the connector. 0131346R $19.95

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Super rugged unit features powerful 3 watt RF amplifier for transmit and sensitive receive amplifier. Utilizes diplexer ceramic filter, Additional circuitry for protection, regulation, etc. Sorry, we have no specs on this, but it’s a treasure trove for the experimenter and RF guru. Brand new. Size: 4.5 x 5 x 1.5” in rugged extruded aluminum heat sink style package. Uses mini UHF connectors. 0127460R $14.95

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Brand new HP Agilent model LST2829 Laser transmitter module. Capable of 622 MB/s data rates, 1 mw output power, 1300 nm wavelength, includes on chip power monitor diode. These are high end quality lasers and not often found on the surplus market! Two style available: A: 32” long thin pigtail fiber and B: 16” long thin pigtail fiber. Each has the same electrical specs. Price: $9.95 each Item A: 0128520R Item B: 0128536R

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In this column, I answer questions about all aspects of electronics, including computer hardware, software, circuits, electronic theory, troubleshooting, and anything else of interest to the hobbyist.

Feel free to participate with your questions, as well as comments and suggestions.

You can reach me at: TJBYERS@aol.com

What's Up:
Confused about coils?
Let me set you straight.
It's too cold to be hot — two thermostat controllers.
Ozone alert. The grid dip revisited and a power supply upgrade.
Don't miss NASA's new cool website.

Wind Your Own

Q. I heard that there is a formula that can help you wind coils by putting the values of diameter, length of coil, and numbers of turn into an equation. What is that formula? Will different sizes of the wire affect the coil? Please give me an example, if you can.

V. Stark via Internet

A. Of all the disciplines associated with electronics, inductance is undoubtedly the least understood. Unlike Ohm's Law — which contains just two variables — inductance is a mixture of physical sizes, shapes, and voodoo magic. To answer your question, all we have to do is look at the equation for calculating inductance, shown in Figure 1. As you can plainly see, inductance increases as the diameter increases — strange, but true.

Now let's wind a 250 µH coil on a 1” x 2” form. The formula for that is:

\[ N = \sqrt{\frac{1}{\mu H(9R + 10L)}} \]

\[ N = \sqrt{\frac{250(9 \times 0.5 + 10 \times 2)}{0.5}} \]

\[ N = 157 \text{ turns} \]

The same 250 µH coil on a 2” x 2” form is:

\[ N = \sqrt{\frac{250(9 \times 1 + 10 \times 2)}{1}} \]

\[ N = 85 \text{ turns} \]

Now, let's deal with the second part of your question — wire size. The diameter of the wire determines how many turns you can wind on a coil form per inch. It also determines the resistance of the coil and the maximum amount of current you can run through the wire before it burns up.

Let's take the turns per inch first (refer to Table 1). From the chart, the largest wire you can use for the 1 inch coil form is 29 gauge or 24 gauge for the 2 inch form. Of course, you can use smaller wire. If you do, though, you'll need to spread the turns apart so they occupy the full 2 inch length.

The resistance of the coil — which is proportional to the length of the wire — is calculated by multiplying the circumference of the form by the number of turns. In the case of the 1 inch form, the circumference is about 3.1 inches for a total length of 493 inches or 41 feet for a resistance of 3.4 ohms (8.183 x .41 = 3.35). The 2 inch form has a resistance of 1.14 ohms (you do the math). The maximum current is 1.2 and 3.5 amps, respectively.

More Wind Your Own

Q. I recently ran across a project that called for a multi-layer RF choke. It would seem to me that placing layers in parallel, one atop the other, would decrease the inductance, not increase it. I'm referring to the parallel inductor formula shown here. Can you clarify this for me?
L\text{total} = \frac{L1 \times L2}{L1 + L2}

C. P. Davis
via Internet

A. You’re confusing series inductors with parallel inductors. When you wind more than one coil with a single strand of wire — either side by side or one atop the other — it’s a series inductor. If the inductors are magnetically shielded from each other, the total inductance is:

L\text{total} = L1 + L2 + L3 ...

However, it’s virtually impossible to prevent coupling between magnetic fields. When you purposely wind one coil on top of another, the mutual coupling becomes even greater. The total coupled inductance of a multi-layer coil can be determined by the formula below, where M is the mutual coupling factor between the coils.

\[
L\text{total} = L1 + L2 + M(L1 + L2)
\]

There are several formulas for calculating the number of turns required in any given application and the results often differ a lot from one formula to another. I use the Wheelers formula for multi-layer coils. Find it in Figure 1.

The formula assumes an air coil. A ferrite core will reduce the number of turns by 10% to 25% — depending upon the bulk and permeability of the ferrite material. A long ferrite rod can reduce the number of turns by as much as 50% to 60%. A brass tuning slug will increase the number of turns by 5% to 10%.

Cooling Fan Controller

Q. I would like to make a control circuit that would turn on a cooling fan whenever my air compressor starts up. After the compressor shuts down, I would like the cooling fan to continue running for a time to completely cool down the compressor.

I was thinking of controlling the fan using temperature monitoring. I could mount a temperature sensor onto the compressor. When the sensor went above a preset temperature (say, 100°F), the cooling fan would start. When the compressor temperature dropped below this setting, the cooling fan would turn off. It would be nice to have the turn on and turn off temperatures adjustable. What do you think?

Bill Blackburn
via Internet

A. I think it’s an excellent solution because it takes into account ambient temperature — which can make the cooling more or less efficient. I suggest the venerable LM56 (or DS56) thermostat IC. It’s small — so you can easily attach it to the compressor — requires few external parts, and is resistor programmable.

Inside the LM56 are two thermostat switches — digital outputs that switch between high and low according to a set temperature point. For this application, we only need one of those switches. The circuit requires just six external components — including the relay (Figure 2).

The relay coil is rated 5 volts at 20 mA — such as the RadioShack 275-232. The contacts are rated 125 VAC at 1 A, so use them to switch the fan’s relay rather than the fan motor — which will likely melt the contacts unless it’s a small fan.

Resistors R1 and R2 set the temperature point. The set points for this circuit are 111°F (44°C) on and 102°F (39°C) off. The following equations calculate the R1 and R2 values for other temperatures:

\[
VT1 = (6.2 \, \text{mV} \times \text{temperature}) + 395 \, \text{mV}
\]

\[
R1 = \left( \frac{VT1}{1.25} \right) \times 25k
\]

\[
R2 = 25k - R1
\]

Make sure you convert the millivolts into volts when calculating R1 and R2. The difference — hysteresis —
between temp on and temp off is internally set at 9°F (5°C).

**I’m Thirsty, Water Me**

Q: Cold weather has forced me to move my potted plants indoors. Now, I’d like to build a plant-watering monitor so that I know when a plant is thirsty and when it’s feeling fine. I saw a Plant Watering Monitor kit in a UK catalog, but the value difference between the Sterling pound and US dollar, along with the shipping, is enough to discourage me from buying it. (The total is about $55.00.)

Basically, it has an LED for “Water OK,” one for “Needs Water,” and one for when the batteries (four AA cells) are low. It advertises a long battery life by flashing the LEDs rather than have them run steady-state. Do you have an equivalent design that I can make with readily available parts? No microcontrollers, please.

L.A.S. via Internet

A: What you ask for can be done using a single LM339 comparator chip (Figure 3) that sells for less than $0.50. The first of the four comparators senses the moisture of the soil by measuring its conductivity (resistance). The “Sensitivity” control lets you set the trip point for a wide range of soil types and moisture conditions.

When the plant is happy, the output of the comparator is high—which, in turn, lights the “Happy” LED. As the resistance of the soil increases—loses moisture—the comparator output flips to the low state and lights the “Thirsty” LED. The “Low Battery” comparator is biased so that, when the battery voltage drops below 4.0 volts, the LED lights.

To extend battery life, I’ve powered the comparator chip and LEDs with a voltage that’s off for about 4 seconds and on for 1/3 of a second using a CMOS LMC555 astable multivibrator. That is, every four seconds, a voltage is applied to the LM339 and LEDs for 1/3 of a second—a flash—resulting in a duty cycle of 8 percent. The average current draw is typically 400 µA—which means your AA cells will easily last through the winter. Increasing the 47 µF cap to 100 µF will nearly double the battery life.

**Surplus NiMH Batteries**

Q: I bought some bargain AA sized nickel-metal-hydride (NiMH) batteries that I found on sale at a surplus outlet. I’m wondering if they can be recharged in a unit I have that is made to recharge nickel-cadmium (NiCd) batteries. Or do they have some fancy controller charge requirements?

Dale Blackwell via Internet

A: I bought a bunch of them myself from All Electronics Corp. (888-826-5432; www.allelectronics.com). Battery capacity is rated in mAh (milliampere-hours). The capacity of the NiMH AA cells on the surplus market is between 1,100
and 2,200 mAH. The 1,800 mAH cells I have state right on the case of the battery that they should be charged with 450 mA for 5 hours or 180 mA for 14 hours — after which they have to be disconnected from the charger.

However, these currents and times assume the cell is fully discharged. If it's only half-used, then these times will overcharge the battery. Once a battery is fully charged, it produces gas — creating a high internal pressure and a sudden rise in temperature. At this point, the battery will begin to vent and release its electrolyte — which severely shortens the life of the cell.

As a rule, a NiCd battery charger can be used to charge a NiMH battery — provided the charger has a two-step charging routine. This class of chargers first applies a fast charge of C/4 to 4C (the total capacity of a battery is defined as C), then switches off (or applies a timed trickle charge).

There are two recommended methods of detecting charge termination: using a temperature sensor in the battery pack or using negative ΔV. The temperature technique relies on detecting the sudden rise in battery temperature to shut off the charge. The negative ΔV system relies on the fact that the NiCd/NiMH battery voltage peaks and drops about 20 mV per cell when fully charged.

Quality chargers use a mix of both methods, called ΔV/ΔT. Cheap battery chargers can't afford this much circuitry and simply place the battery on prolonged trickle charge (typically C/10) in the hope that it doesn't do much damage.

**This Old House Thermostat**

My house has an open stairwell between the main floor and the basement, where I have an office and my electronics workshop. When the weather is neither too hot nor too cold, the circulating fan on the heat pump stays off for long periods. The cold air gravitates down and the hot air goes up, creating an uncomfortable condition in both places.

Eventually, the thermostat detects this and the fan starts. To correct the problem, I built 555 timer to cycle the fan. This helped a lot, but ran the fan at the wrong time in the summer.

I then built a differential temperature device using two thermistors, an op-amp, and a relay. Unfortunately, my design was not sensitive enough — the temperature spread was too great. I kept changing feedback resistors, but was unable to get it right. I would like to build a controller that I can comfortably adjust to a 1 to 4°F differential.

C. P. Furney, Jr. Loudon, TN

Maybe your problem is that thermistors are non-linear. That is, the resistance doesn't stay in step with the temperature. Let's replace the thermistors with the venerable LM34 temperature sensor (shop around for best price; it can vary widely). The LM34 is a precision Fahrenheit temperature sensor with a guaranteed 10 mV/F linear output (80 mV at 80°F, 100 mV at 100°F).

Now, if you place two LM34 sensors on the differential inputs of an op-amp (any garden variety will work), you automatically get a voltage that reflects the difference in temperature between the upstairs and downstairs (Figure 4).

This voltage is first multiplied by 10 and then fed to a comparator with an adjustable temperature differential (SET) up to 10°F. This should give you enough range between upstairs and downstairs so that the rooms don't become uncomfortable.

The 1M resistor provides a slight amount of hysteresis to prevent the fan from hunting — constantly going on and off. If you find the fan hunting, lower the value of the 1M resistor. To clarify: The SET determines the temperature difference between the basement and upper house. The 1M (feedback) resistor determines the temperature difference between fan on and fan off — a dead band that prevents hunting.

**Grid Dip Revisited**

Q: About the “Dip Oscillator Meter” in the January 2005 issue ... I pretty much have most of the parts, except for the variable capacitor. Do you know where I can find those variable capacitors?

James Ko via Internet
I know they are not easy to find but they are plentiful in old radios of all kinds. The best source is from antique radio sales, like Surplus Sales: www.surplussales.com/Variables/AirVariables/AirVar1.html (CAV) MAPC-50ME. Can’t afford these treasures, you say? Try the circuit in Figure 5.

In place of the mechanical variable capacitor is a semiconductor varactor diode. A varactor is a reverse-biased diode that changes capacitance with voltage. The greater the voltage, the lower the capacitance. FYI — any diode can be used as a capacitor in the reverse-bias mode. The varactor is special in that it has predictable characteristics. You may notice that the schematic isn’t complete — I’ve just highlighted the varactor section. For those readers who missed the original design, I’ve posted it on our website (www.nutsvolts.com) under GRID_DIP.PDF.

**Grid Dip Meter Varactor Tuning**

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I have a smoke detector in the garage, but I cannot hear the beeper with the door shut. I tried using one of the Ramsey kits, “The Voice Switch (VOX).” When I use it with a relay and small siren, it works, but you have to reset it manually. Can you help me?

Pete Thedoulou
via Internet

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Think about it for a minute. The VOX is activated by the sound of the smoke alarm, right? So when the siren goes off, what does it produce? Louder sound — sound that prevents the VOX from turning off. The best way to prevent this is to pulse the siren on and off to break the loop. This can be done using a car alarm that you can buy at an auto parts store or by using the circuit in Figure 6.

This is a simple 555 astable timer with an on/off time period of about two seconds that drives a relay (RadioShack 275-005) to pulse your siren. Not only does it break the feedback path, but a pulsating alarm draws more attention than one that just screams. To minimize feedback from the siren, attach the microphone as close to the smoke detector as possible, maybe with duct tape.

---

**Cool Websites!**

Every month, I collect websites that are cool, safe, and fun and publish them in a monthly newsletter. Here, you will find my past monthly newsletters. — Mark Donaldson

www.geocities.com/luem42/newsletter.html

Take NASA’s interactive “Planet Quest” quiz to see if you know what is fact and what is science fiction.

http://link.abpi.net/l.php?20041123A6

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www.bleacheatingfreaks.com/flash/games/popoint.html

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The Wart Remover originally came about by accident. I had a local infection, which was thought to be “hiding” from antibiotics, and so I sought to treat it with Crane frequencies — a range of electrical frequencies which supposedly destroy specific microbes.

Without knowing what voltage or current to apply, the treatment was surprisingly and completely successful. However, it caused a little damage to the skin. What if, I thought, Dr. Crane’s frequencies would cause similar damage to warts?

My first experiments met with some success, however, the results were patchy. There were unexpected failures which, at that stage, were not understood.

After designing five successive prototypes over a period of a year, I finally achieved the desired consistency and the final prototype (described here) worked without fail on small- to medium-sized warts.

A number of prototypes were tested on several volunteers, as well as being loaned to two doctors. These achieved close to 100% success with the common wart (a brown or skin-colored, rough wart) and 100% success with the plane wart (a very flat wart).

This does not, of course, guarantee that the Wart Remover will work in every case. However, it does offer reason for hope that the device would be effective in a great many cases.

Medical History

During the 1950s, Dr. John Crane established that a frequency close to the one used in the present design was one ideally suited for treating warts and the wart virus. This frequency is used here with suitable voltage and current. However, since Crane frequencies may not be the full explanation for the Wart Remover’s success, the theory is discussed in more detail in the sidebar.

While researching this project, I found two Crane frequencies for warts (2.127 kHz and 21.27 kHz) and empirically settled on the higher frequency.

It has since been questioned whether Dr. Crane’s frequencies are at all significant or whether any frequencies within a few 100 or even 1,000 Hz would work just as well. I chose Dr. Crane’s original frequency and, assuming that this is optimal, close frequencies and harmonics might yield similar results.
It is interesting to note that Dr. Crane’s frequencies for cancer (sarcoma and carcinoma) lie close to those for warts. This raises the possibility that the Wart Remover might work for certain cancers. However, the Wart Remover would not be recommended in such a case, since one cannot afford to take chances with personal experiments on cancers.

**Wart Removal Today**

Removing warts has never been much fun and the use of the Wart Remover is likely to be painful — but only briefly and not too much so.

One of the most common methods of removing warts is liquid nitrogen treatment (also called cryosurgery or “controlled frostbite”). However, this is both painful and messy. Not only that, but it may be counterproductive, in that it may worsen the treated warts in the long run. It sometimes does permanent damage to the skin (particularly darker skin) and poses a far greater risk of infection.

A more modern method of removing warts goes by the name electrodesiccation (or sometimes, “radio frequency thermal ablation”); that is, burning off warts electrically.

This is far more tidy and is quicker than the method presented here. However, it tends to be expensive and is unavailable to people in less developed or more remote areas of the world. Also, it typically uses 1,000 times more power than this circuit and could be dangerous to try to implement as an amateur project. The Wart Remover thus brings the destruction of warts within the scope of the amateur constructor.

As improbable as it may seem, the common wart may be destroyed with a simple circuit that uses a tiny key chain battery delivering a boosted 24 volts to the skin. Taking into account the resistance of the skin, this translates to just 100 µA or so passing through the wart internally, thus delivering a fraction (about 1/4) of the peak power delivered by a typical TENS unit.

For the price of a doctor’s consultation for the dreaded liquid nitrogen treatment or for the price of a single session of electrodesiccation, several Wart Removers could be built. Moreover, a single key chain battery should be sufficient to destroy as many as 40 or 50 warts.

**Safety and Caution**

Despite the very small currents used by this circuit, little is understood about the effects of electricity on the human body and the Wart Remover should be used with this caution in mind. In early experiments, while I was still seeking to establish the correct “exposure” required to destroy a wart, I caused temporary damage to a nearby fingernail, which “warped” until the fingernail grew out again. Similarly, an Internet site reported stiffness in a finger joint that was subjected to a related treatment.

These are relatively minor side effects, yet it should be kept in mind that the Wart Remover is capable of doing some damage if misused. Therefore, the voltage, current, frequency, and duration of treatment described in this article should not be rashly modified. A year’s experimentation lies behind this design and most — if not all — of the mistakes have hopefully been made and addressed.

**Practical Experience**

During testing, virtually all common warts and plane warts were ultimately removed, but there were some differences in the effect that the device had. In several cases, a wart was obliterated the first time, never to return. These were usually small, common warts, less than 4 mm in diameter. However, with close constellations of warts (at first glance looking like a single wart) or with larger warts, the wart was sometimes destroyed in part, but needed follow-up treatments (or a few treatments at once) to destroy all of it.

During testing, only one wart proved to be really difficult to remove; in this case, it measured a whole 12 mm across. After four treatments in quick succession, it was significantly reduced in size, but was still some way from complete destruction. This wart had, in fact, been worsened by liquid nitrogen treatment.

In almost every case, little or no pain was experienced when the Wart Remover was first applied, although one subject jumped when the device was first switched on. This should be avoided in this design with a small modification described later in this project.

After a certain period of painlessness, which varied from about 1/2 a minute to 3-1/2 minutes, subjects suddenly felt a burning or even “spine-chilling” pain inside and under the wart. This pain only lasts about half a minute, then subsides. However, it is necessary for the removal of the wart and needs to be endured. When the pain has subsided (or after 5 minutes, whichever may come first), the electrode is removed.

It should immediately be apparent that the wart is “just
In many cases, the wart melted with a fizzle even before treatment was over. The skin immediately surrounding the wart may be irritated for a few hours and there may be a slight swelling around the wart. Ultimately, a scab is likely to form and, perhaps three weeks after treatment, the wart should “expire” and come off — or, in some cases, partly come off. Don’t remove a wart too soon or break its surface, since this could leave a deep wound and infection could represent a risk. If it is left alone, there should be no infection.

If a treatment should have little or no effect, it would be sensible to consult a doctor.

The Circuit

The Wart Remover uses a single 4060 CMOS oscillator IC (see block diagram Figure 1), which incorporates a 14-stage binary divider. I chose this IC for its simplicity (it incorporates the oscillator), for the square wave outputs provided by its internal divider, and its ability to have three separate outputs employed for three separate purposes.

The fourth-stage output (pin 7) switches a solid-state switch (a power MOSFET) to pulse 24 volts through the electrodes at the required frequency. The fifth-stage output (pin 5) powers a voltage booster (12 to 24 volts — see the top of Figure 1) and the sixth-stage output activates a peizo sounder that gives a direct indication that the oscillator-divider IC is working.

One of the electrodes is positive (+24 volts, called the dispersive electrode and labeled DE) and may either be a metal grip held in the hand or a metal plate applied to an area of skin near a wart. The other electrode is negative (0 volts, called the active electrode and labeled AE) and this is a sharp(ish) metal point used for direct contact with the wart.

I settled on a 24 volt, 21.27 kHz square wave (or thereabouts), applied to a wart for five minutes. I found that pulses of 1 mW power (minimum) passing through the wart internally were required to achieve any effect and that 3-6 mW pulses were adequate.

Current across the probes (see Figure 2) is limited by R4 to 2.4 mA (maximum) so as to protect the circuit if the probes should be short circuited. One needs to also factor in the conductivity of the flesh and this rarely falls below about 200K; therefore, little more than about 100 µA would course through the wart itself.

The frequency of the oscillator section is roughly calculated by the formula f=1/(2.2 x R1 x C1), although this becomes undependable, in practice, at higher frequencies. I selected the Philips HEF4060BP IC for U1. Note that different makes of this IC can affect the frequency and, if a different make is used here, I would suggest that the frequency be adjusted with the help of a frequency meter (adjust the value of R1). Having said this, frequency is unlikely to be critical.

Q1 provides an efficient switch for pulsing the voltage through the flesh and may be almost any power MOSFET. I used an IRF823 that I obtained in an All Electronics bargain pack — presumably a high voltage device in the IRF series. The more common IRF510 would serve just as well. C4 serves as a supply decoupling capacitor and S1 as an on-off switch.

Some “trappings” are added for convenience and comfort. Most importantly, a 470K potentiometer is inserted in the dispersive (+24 volts) electrode’s lead and may either be a metal grip held in the hand or a metal plate applied to an area of skin near a wart. The other electrode is negative (0 volts, called the active electrode and labeled AE) and this is a sharp(ish) metal point used for direct contact with the wart.

For those who are likely to use the device more often, a standard “battery low” circuit could also be added. Lastly, the fifth-stage output is used to raise the battery’s 12 volts to 24 volts by means of a standard voltage doubler. The circuit is thus directly powered by 12 volts, while a boosted 24 volts is switched through Q1 to the electrodes. Most importantly, this boosted voltage helps the circuit overcome skin resistance, so that it is able to provide the
**Wart Remover**

**Theory and Practice**

Theory has it that alien cells, such as wart cells, begin to resonate when bombarded with a specific electrical frequency — much as a peizo sounder resonates most intensely at its resonant frequency. Normal chemical processes at the cell boundary are thereby disrupted (or the cell ruptures), thus killing the cell. Healthy tissues are left relatively unscathed.

However, this is not the only theory in the running. By way of a process of elimination, I followed up further suggestions put to me by leading researcher Aubrey Scoon:

1. Electrolysis. I found that electrolysis (using a “flat” DC voltage) also had a significant effect on warts; however, this did immediate superficial damage to healthy tissues, as well. My conclusion was that electrolysis — this theory appeared to be ruled out. It also seemed to be contradicted by the sometimes spectacular action of the Wart Remover.

2. Iontophoresis. This is the leaching of ions into the wart, which would effectively poison the wart. However, after experimenting with ferrous, non-ferrous, and graphite probes — all of which were tried with success — this theory appeared to be ruled out. Also seemed to be contradicted by the sometimes spectacular action of the Wart Remover.

3. The stimulation of immunomodulatory chemicals. The theory is that these chemicals, when stimulated by an electrical frequency, attack the wart and destroy it. This, however, would seem hard to explain in light of the spectacular destruction of several warts, some of which fizzled up before my very eyes.

4. Frictional heating. Ionic agitation may raise the temperature within the wart, causing tissue coagulation. While I had no way of testing this theory, I thought it to be unlikely. Existing electrodessication equipment typically burns off warts with a few watts of power, raising the temperature within a wart above the 47°C required for the denaturation of tissue proteins. However, since the Wart Remover pulses just one-thousandth as much power through a wart, this possibility was not considered a leading contender.

3-6 mW power necessary to destroy a wart internally. As the voltage is raised, the power pulsed through the wart increases, as is confirmed by the equation I=V/R.

3-6 mW power necessary to destroy a wart internally. As

Construction

The Wart Remover is built on a printed circuit board (PCB) measuring approximately 2-1/2” x 1-1/2” (see make of the battery.

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Figure 3). As is seen from the photographs, the prototype could be built into a very small case. It should not be difficult, in fact, to redesign it to fit into an oversized pen.

Solder the battery holder to the PCB (two 8 mm crimp terminals), attaching a round head (No. 2) paper fastener to the negative (0 volt) crimp terminal. Alternatively, the battery may be soldered directly to the PCB by means of two solid-core wires; this must be done quickly to avoid overheating. Solder the six solder pins and the 14-pin dual-in-line (DIP) socket to the PCB. Take note of the DIP socket's orientation. Solder the resistors to the PCB, the capacitors (take note of the orientation of C4), the diodes, and Q1.

Insert the PCB in the case as shown. Mount on-off switch S1 on the case and connect it as shown (this should be switched off to begin with). VR1 is attached by an end terminal to the solder pin and its wiper is taken to the dispersive electrode, so that its resistance decreases when the shaft is turned clockwise. Peizo sounder X1 is attached to the solder pins.

Drill a hole in the case next to the switch, through which the wire to the dispersive electrode (a metal grip or metal plate) will be passed. Make sure that there is a sound electrical connection with the metal grip or plate. Then drill a hole for the active electrode, which is inserted through the end of the case and soldered to the two solder pins. This probe may be a needle with its sharp point filed off with a fine file to make a sharp(ish) stub.

Drill holes on the lid of the case for VR1 and the peizo sounder, gluing the sounder over the hole so that its sound escapes through the hole. Insert U1 in the DIP socket, observing anti-static precautions (first touch your body to ground). The whole PCB, if desired, may be secured in the case with a little epoxy glue. Be sure to insert the battery the correct way in its holder, since the circuit has no reversed polarity protection; a mistake here could destroy the circuit. If there are any problems on completion, the first suspects should be Q1 and U1.

### In Use

A year of experimentation preceded the development of this circuit and the results gave me a new respect for the potential risks of electricity, however small the voltages and currents which are applied.

Skin resistance can vary between about 100K and 8M, depending on the day and the situation. Therefore, to ensure consistency of results, skin resistance needs to be kept relatively low. Use a little skin moisturizer where the skin makes contact with the dispersive electrode, as well as a little moisturizer on the wart itself.

Constructors are advised not to use the circuit where current would flow across the head or the heart and never in a case where a person uses a pacemaker or has any history of epilepsy. All the precautions that apply to a TENS device apply also to the Wart Remover.

When treating a wart on, for example, the lower or upper arm, hold a metal grip (the dispersive electrode) in the same hand. If it is not convenient to use a grip, rest the limb to be treated on a metal plate that is again connected as the dispersive electrode.

The active electrode, which is a sharp metal point (but not too sharp), is rested directly and gently on the top of the wart. If the wart is large (say 5 mm or more in diameter), it might be a good idea to tackle one or the other side of it first, since the Wart Remover is unlikely to kill all of it at once.

Switch it on and apply the Wart Remover to a wart for up to five minutes, then switch it off. If desired, use VR1 as described to avoid any initial jolt and be prepared to suddenly experience perhaps a minute of sharp pain. If you do not see this through until the pain subsides, the wart may not be destroyed.

The Wart Remover came as a welcome relief to my son, who couldn’t bear the thought of further treatment with liquid nitrogen. He claimed that the Wart Remover was far preferable and that the pain was “not bad” in comparison.

While this circuit comes with no guarantees, it is nothing ventured, nothing gained! With several willing “guinea pigs” and further volunteers queuing up, I found that the Wart Remover was entirely successful, most of the time. **NV**

---

### Parts List

<table>
<thead>
<tr>
<th>Resistor</th>
<th>Value</th>
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</thead>
<tbody>
<tr>
<td>R1</td>
<td>5K ohms</td>
</tr>
<tr>
<td>R2, R3</td>
<td>100K ohms</td>
</tr>
<tr>
<td>R4</td>
<td>10K ohms</td>
</tr>
<tr>
<td>VR1</td>
<td>470K ohm miniature linear potentiometer</td>
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<table>
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<tr>
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</tr>
<tr>
<td>C2</td>
<td>220 nF</td>
</tr>
<tr>
<td>C3</td>
<td>100 nF</td>
</tr>
<tr>
<td>C4</td>
<td>100 µF electrolytic 16 V</td>
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<tr>
<td>D1, D2</td>
<td>1N4001</td>
</tr>
<tr>
<td>Q1</td>
<td>IRFB23 (or IRF510, BUZ11, etc.)</td>
</tr>
<tr>
<td>U1</td>
<td>HEF4060BP (or equivalent — see text)</td>
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<table>
<thead>
<tr>
<th>Miscellaneous</th>
<th>Value</th>
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</thead>
<tbody>
<tr>
<td>XI</td>
<td>Peizo sounder (without internal electronics)</td>
</tr>
<tr>
<td>S1</td>
<td>On-off switch</td>
</tr>
<tr>
<td>B1</td>
<td>23 A or MN21 12 volt key chain (“remote”) battery</td>
</tr>
</tbody>
</table>

- Two 8 mm crimp terminals for battery holder
- Round head (No. 2) paper fastener for battery holder
- 6” long x 0.4” diameter brass pipe for dispersive electrode
- One yard insulated wire to dispersive electrode
- 1.6” needle for active electrode

- 2-1/2” x 1-1/2” copper-clad board, small ABS plastic enclosure, four-pin dual-in-line (DIP) socket, epoxy glue, eight solder pins, solder, etc.
FEBRUARY 2005

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Here’s a great start for a solar cell project. From not-yet-assembled solar-powered garden lights, these assemblies include two glass photovoltaic cells mounted on a plastic base. Output is approximately 2.6 Vdc @ 25 mA in bright sunlight. Under the photocells is a bracket for a two cell rechargeable AA pack & a small circuit board with three red LEDs. There is a photoresistor on top of the panel between the solar cells to sense light and dark conditions. In daylight the cells charge the battery. When it gets dark, the LEDs light. These are working units but the batteries packs are old and may not take a charge. Our two AA cell nickel-metal-hydride pack, CAT# NMH-2AA ($2.00 ea.) is a good replacement. Solar cell surface area: 3.78” X 1.98”.
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J.S. Popper “Bed-of-nails” test clips with insulating boots on approximately 46” long leads. Bed-of-nails clips have multiple spikes in the middle of the clip enabling measurement through insulated wire. The jaws at the front of the clip grab and hold securely to plugs or terminals. The leads are stranded copper litz wire with red and black woven cloth insulation. Leads were cut from new equipment and may require a crimp terminal to facilitate attachment.
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Shogyo #3650VC. Solid-state audio indicator emits a medium-loud, high-pitched tone. Screwdriver adjustable trimmer on back of device controls volume. Operates on 4-28 Vdc @ 6 mA. Black plastic face is 1.45” diameter x 0.16” thick. 1.25” diameter threaded mounting bushing with large plastic nut mounts in panels up to 0.5” thick. 0.187” qc or solder terminals.
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FAN-COOLED 6-12 VDC MOTOR
Smooth, powerful DC motor with internal cooling fan. Operates on 3-12 Vdc. 11,500 RPM @ 6Vdc, 1.35 Amps. 1.45” dia. x 2.25” long. 0.125” diameter flatted shaft is 0.7” long. Two threaded mounting holes on face of motor on 1” mounting centers. Solder lug terminals.
CAT# DCM-231 10 for $3.50 each 75 for $3.00 each
Are you looking for a programmer that fits in your wallet? It’s here! Figure 1 shows a tiny device programmer that is only the size of a business card, but can be used to program Atmel’s many AVR microcontrollers (MCUs). More importantly, it doesn’t use its own software to work, but instead uses the host computer’s existing software, a terminal emulation program. So only the programmer hardware and firmware need to be designed — no software for the host operating system needs to be developed or installed. This feature not only simplifies the development process, but also makes the programmer independent of the host operating system. As a result, the programmer can be used on any host computer platform — from Windows to Linux or Unix — as long as the latter has a terminal emulation program. For Windows PCs, this program is called HyperTerminal; I will explain it more later.

The programmer also has an interesting feature: Its hardware resource can be used to demonstrate some sample programming results, so you don’t have to build your own test circuit. Such a unique feature is a great boon for users.

The AVR Advantages

Atmel’s AVR MCUs feature enhanced RISC (Reduced Instruction Set Computer) architecture offers the highest MIPS-per-milliwatt capability for the eight-bit MCUs that has been introduced to the market with a variety of derivatives. The demand for these MCUs is still growing. Compared to the old eight-bit MCUs — such as the 8051s — a major advantage for the AVR is that it can be programmed in-circuit. This is achieved by its SPI (Serial Peripheral Interface) programming approach. Any AVR MCU has an SPI serial port comprised of three pins (SCK, MISO, and MOSI) for in-system programming, among other features. This makes the AVR programming very simple and easy. We’ll see this in the next section.

Circuit and Operation

Figure 2 shows the schematic of the AVR HyperTerm programmer. It consists of only two chips: Dallas Semiconductor’s RS-232 transceiver chip DS275 (U1) and Atmel’s 20-pin AT89C2051 microcontroller (U2). U3 is a 20-pin socket used to hold the AVR MCU to be programmed; it can be either AT90S1200 or AT90S2313. U1 functions as an RS-232 signal level translator that translates the signal levels between TTL and RS-232 and vice versa. Dallas Semiconductor’s DS275 is used because it has an advantage over the MAX232 chip, since the latter is bigger (16-pin) and needs five electrolytic capacitors to work. Here, we don’t need a capacitor, but use a Schottky diode IN5817 with DS275 for latch-up protection. Latch-up can occur if the power supply for DS275 has been discontinued while communication is still taking place. In that situation, the Schottky diode will first conduct (because it conducts at a much lower voltage 0.3 V) to protect the DS275. You can order the DS275 chip from Dallas Semiconductor/Maxim’s website at www.maxim-ic.com.

U2 is the heart of this programmer that handles communication with the host computer and all programming chores. The AT89C2051 is chosen because of its wide availability and it is a “minimized” 8051, so many people are familiar with its instructions. It has 2 Kbytes of Flash memory to store the program code — known as firmware. That is enough for our purpose and only four control pins (P1.7 to P1.4) are needed for AVR programming because of the SPI feature.

From Figure 2, we see that port pin P1.7 is used to reset the AVR after power-up, P1.6 generates the required clock signal for data transfer between U2 and U3. P1.5 connects to the AVR’s MISO (Master-In-Slave-Out) to read data from the AVR, and P1.4 outputs data to the AVR’s MOSI (Master-Out-Slave-In). Note that the AVR is a slave device.
during programming; it needs a crystal or ceramic resonator, CR1, for data movements.

Power supply for the programmer is drawn from a 9–12 V wall wart via a 78L05 voltage regulator to produce 5 V. Capacitor C1 is used for smoothing. C2 is for resetting U2. C3, C4, and the 3.6864 MHz crystal provide the micro with the required working frequency. LED1 is used to indicate the circuit’s working status. C5 is for decoupling. That is all there is to the programmer circuit description. It’s quite simple, consisting of only two small chips. The AVR’s serial interface makes it easy to program and there are still alternatives for the circuit. For example, you can use a MAX232 if you don’t have a DS275 on hand; also, you can use another 8051 micro for U2 — such as AT89C51/52 or P87C51/52. The only drawback is that these chips are bulky, but they work just fine.

**Construction**

The construction for this programmer is also quite flexible. Depending on what chips and materials you are going to use, you can build it different ways: on a solderless breadboard, a perforated board, or using a PCB (Printed Circuit Board).

For the people who prefer to build a permanent gadget, you can download the foil patterns of a double-sided PC board from the *Nuts & Volts* website at [www.nutsvolts.com](http://www.nutsvolts.com). You can make your own PCB or get one from the source given in the Parts List. By inspecting Figure 1 and the PCB layout, it’s easy to identify each component’s location and orientation or polarity. When inserting a diode or electrolytic capacitor into the PCB, care must be taken not to make a polarity error.

The AT89C2051 (U2) must be programmed before mounting it on the board. The firmware is an Intel hex file — AVRTMP1A.HEX — which can be downloaded from my website at [www.geocities.com/xumicro](http://www.geocities.com/xumicro). You can “burn” this chip with the firmware file if you have an 8X51 programmer; otherwise, you can purchase it with the PCB.

For either building it on a perf-board or PCB, the basic principles are the same. Depending on your programming and financial considerations, it can be built in either a deluxe version or an economic version. For the deluxe version, use solder-tail IC sockets for chip U1 and U2, but a 20-pin ZIF (zero insertion force) socket for the AVR MCU. Because the ZIF socket costs about $10.00, you can replace it with the regular

---

**Figure 2.** The AVR HyperTerm schematic.

**Figure 3.** Adapter circuit.

**Figure 4.** LEDAVR hook-ups.
20-pin socket, but that will compromise some flexibility. After you solder all sockets and other passive components onboard and test each Vcc pin on the sockets to make sure that they actually deliver 5 V, remove power and mount the ICs. If everything goes normally, LED1 should light up after power-on.

It should be emphasized that this programmer — when it is built in the deluxe version — can program not only the 20-pin AT90S1200/2313, but also the eight-pin AT90S2323/2343 and the 40-pin AT90S8515. The only thing you need to do is build the appropriate adapters for them.

As an example, Figure 3 shows the adapter circuit for eight-to-20-pin conversion. Because each AVR uses four pins (*RESET, SCK, MISO, and MOSI) for its programming, transforming these pins from 20-pin sockets to eight-pin sockets makes it possible to program the eight-pin AVR, as they have similar architecture.

To actually build this adapter, you can use two pieces of small perfboards, one 20-pin wire-wrap socket (its pin legs should be 0.5" long), one eight-pin solder-tail socket, and some wires. First, insert each socket onto each perfboard and solder it in place. Then, use spacers or standoffs and nuts to stack them together with the eight-pin socket on top and fix them. The perfboards should be cut small enough that the adapter can be easily plugged into the programmer’s ZIF socket.

### Firmware Design Ideas

Once the hardware design has been made, the next and most time-consuming part is to design the firmware. That means to write the program for microcontroller (U2) to handle communication with the host computer and the programming chores of the AVR. A few important points must be outlined first.

The first task is to decide on the RS-232 communication settings with the host. We chose a Baud rate of 9600 bps, eight data bits, none parity, and one stop bit. These are the commonly used serial communication settings: 9600 bps, 8N1.

When the programmer is powered up, it sends a start-up message to the host screen and displays a command menu like this (extracted from the assembly program):

```
DB 'AVR HyperTerm Programmer'
DB 'Commands:', CR, LF
DB ' ^B: BlankCheck', CR, LF
DB ' ^E: EraseChip', CR, LF
DB ' ^W: WriteFlash', CR, LF
DB ' ^R: ReadFlash', CR, LF
DB ' ^V: Verify', CR, LF
DB ' ^I: ReadID(SignatureBytes)', CR, LF
DB 'Enter your selection (press ctrl key first)', CR, LF
```

When six commands are defined for the AVR programming tasks, each begins with a control key (^). For instance, the user can press ctrl-B to BlankCheck the chip; if the result is shown as “This chip is NOT Blank,” then he/she can press ctrl-E to erase the chip, and so on.

These commands are complete enough to cover the AVR programming tasks; a command to read the chip ID — also known as Signature Bytes — is even included. For each task, a related Command Processing Routine must be written to process the detailed operations.

For simplicity, we chose to transmit/receive only ASCII characters between the host and programmer. The programmer expects to work with a TTY terminal. To control data flow between different speed terminals, we chose the commonly-used software scheme XON/XOFF for Flow Control.

Of the above six commands, only ^W and ^V involve the use of file transfer. We use an Intel Hex format ASCII file to program the AVR or to verify AVR Flash memory contents. Here, XON/XOFF flow control is extensively used during these processes. For example, data is sent byte-by-byte from the host and, when the programmer receives a byte to program (that may take

### Listing 1. The LED1AVR.ASM program source code.

```assembly
; program name: LED1AVR.ASM
; 1 Hz blinking LED driven by AVR working at 4 MHz
; LED is connected to AVR PortD Bit_6 (PortD = $12)
; That is Pin 11 for AT90S1200/2313
.include "2313def.inc" ;Port definitions here
.cseg
.org 0

start:
  ldi    r16, low(RAMEND)   ;\set up sack
  OUT    SPL, r16          ;/
  sbi    DDRD, 6     ;config DDRD bit-6 as output
rept:
  cbi    PORTD, 6    ;LED=ON
  RCALL  DLhalfS
  sbi    PORTD, 6    ;LED=OFF
  RCALL  DLhalfS
  rjmp    rept        ;repeat again
/**
; delay = 1/2 sec at 4 MHz
DLhalfS:
  LDI    R20, 10
calop:  LDI    R19, 255
  LDI    R18, 255
malop:  LDI    R18, 255
  LDI    R19, 255
LOOP1:
  DEC    R18
  brne   LOOP1
  DEC    R19
  brne   malop
  DEC    R20
  brne   calop
  RST
```

When six commands are defined for the AVR programming tasks, each begins with a control key (^). For instance, the user can press ctrl-B to BlankCheck the chip; if the result is shown as “This chip is NOT Blank,” then he/she can press ctrl-E to erase the chip, and so on.

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10 milliseconds), it sends an XOFF character to the host, so the host stops sending until the programmer has completed this byte programming and sends an XON character to inform it. Then, the host continues data sending.

**Setting Up HyperTerminal**

It’s clear from the last section that properly setting up the HyperTerminal for our unique requirements is vital for the programmer to work.

The HyperTerminal program has many capabilities and many options, but we only utilize a few of them. More importantly, many of its “default” settings are NOT what we want. We must change them to match our programmer’s settings.

To find the HyperTerminal program on the PC, begin from the “Start” button, go to Programs > Accessories > Communications, where you can see the HyperTerminal icon, and double-click it. This opens a New Connection. The New Connection dialog box appears and prompts you to enter a Name for it. Type in any name (such as Xtm) and choose an icon, then click OK.

The next dialog box is Connect To. Here, you have to reject and click NO to many default settings: don’t enter any area code or phone number, but, rather, choose the “Connect using Direct to COM1” option and click OK.

Once you’ve chosen COM1, the Port Settings dialog box appears. Select Baud rate and other settings to match the programmer: 9600, 8-N-1; also, remember to select XON/XOFF for Flow Control (reject default “Hardware”). Click OK.

Now, we will deal with the HyperTerminal window displays, but not everything has been set up. Click the File menu under the title bar; find the item Properties. Click it and you’ll see the “Settings” tab within the Properties. You need to change two items in it: Choose “TTY” for the Emulation type and then, in the ASCII Setup menu, put a check mark in the box for “Send line ends with line feeds.” Click OK. You’ve finished with Terminal set-ups.

**Using the Programmer**

After setting up HyperTerminal, you can connect the programmer to COM1 of your PC and power it up. Then, you’ll see the following start-up message appear in a window:

AVR HyperTerm Programmer Commands:

- ^B: BlankCheck
- ^E: EraseChip
- ^W: WriteFlash
- ^R: ReadFlash
- ^V: Verify
- ^I: ReadID(SignatureBytes)

Enter your selection (press ctrl key first)

---

**Parts List**

<table>
<thead>
<tr>
<th>Part</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>C1</td>
<td>100 mF 16 volt radial electrolytic capacitor</td>
</tr>
<tr>
<td>C2</td>
<td>2.2 mF 16 volt radial electrolytic capacitor</td>
</tr>
<tr>
<td>C3, C4</td>
<td>27 pf ceramic capacitor</td>
</tr>
<tr>
<td>C5</td>
<td>0.1 mF ceramic capacitor</td>
</tr>
<tr>
<td>R1</td>
<td>330 ohm 1/4 watt carbon resistor</td>
</tr>
<tr>
<td>U1</td>
<td>RS-232 transceiver DS275 by Dallas Semiconductor</td>
</tr>
<tr>
<td>U2</td>
<td>AT89C2051 Flash microcontroller (programmed)</td>
</tr>
<tr>
<td>U3</td>
<td>AT90S1200 or AT90S2313 AVR to be programmed</td>
</tr>
<tr>
<td>VR1</td>
<td>78L05 voltage regulator IC</td>
</tr>
<tr>
<td>J1</td>
<td>Power jack</td>
</tr>
<tr>
<td>J2</td>
<td>DB9F connector</td>
</tr>
<tr>
<td>D1</td>
<td>Schottky diode IN5817</td>
</tr>
<tr>
<td>LED1</td>
<td>General-purpose light emitting diode</td>
</tr>
<tr>
<td>XTAL</td>
<td>3.6864 MHz crystal</td>
</tr>
<tr>
<td>CR1</td>
<td>4 MHz ceramic resonator</td>
</tr>
</tbody>
</table>

Miscellaneous: 9-12 VDC wall wart power supply, wires, solder, etc.

**NOTE:** The following items are available from G.Y. Xu, P.O. Box 14681, Houston, TX 77021

<table>
<thead>
<tr>
<th>Item</th>
<th>Price</th>
</tr>
</thead>
<tbody>
<tr>
<td>1. Assembled and tested AVRTMP-1 programmer</td>
<td>$34.95</td>
</tr>
<tr>
<td>2. Kit only</td>
<td>$29.95</td>
</tr>
<tr>
<td>3. PCB and programmed AT89C2051</td>
<td>$10.00</td>
</tr>
</tbody>
</table>

Please visit [www.geocities.com/xumicro](http://www.geocities.com/xumicro) for ordering information.
This command generates a listing file LED1AVR.LST and Intel Hex file LED1AVR.HEX, which is what we need for programming and is shown in Listing 2.

To write AVR Flash memory, first press ctrl-W, then go to “Transfer” menu in HyperTerminal, and click “Send Text File.” Enter the file name LED1AVR.HEX in the dialog box and press <enter>. In a moment, the text file transfer and programming will take place and the progress is shown on screen. Finally, you’ll see the “Programming Completed” message.

To verify the programming, use almost the same procedure as Writing, but — this time — first press ctrl-V and then go to the “Transfer” menu and do the same “Send Text File” process. Once you type in a test file name and press <enter>, that file is sent to the programmer and compared with the memory contents being read. If every byte comparison is okay, a “Verification Successful” message displays.

On some desktop or laptop computers, things may not be going so well. If that happens, you may need to redo something on the File menu. For example, if you can’t program all bytes correctly or some bytes are shown as missing when read, then you may need to go back to File > Properties > Settings > ASCII Setup, and put a 1 millisecond delay on both the Line Delay and Character Delay boxes.

Figure 4 shows how to physically hook up the LEDAVR circuit to demonstrate your programming results. This circuit can be mounted on a solderless breadboard. We also provide another program called LED2AVR.HEX to light up the same LED, but with a double blinking feature. You can try it out after programming with LED1AVR.HEX.

You don’t have to hook up any circuits, though, just use the programmer itself to demonstrate your success. Note that both the 20-pin socket U2 and U3 have the same Vcc and GND pins, in addition to the same Reset (pin 1), Oscillator (pins 4 and 5), and LED connect, pin 11. So, after programming, simply remove the AT89C2051 from the socket and replace it with the programmed AT90S1200/2313. Then, power-up and you’ll see the LED blinking or double blinking. This feature of the program saves you time and money.

RJL Systems has a 25 year history in medical devices and is proud to announce an analog development board for engineers and hobbyists who demand accurate signal processing for display and communications.

- Bipolar 16 bit ADC (+/- 1.5000 volts FS 100K SPS)
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- Isolated power supplies (+/- 5.0V analog and 5.0V digital)
- Isolated 9 digital PIC I/O pins with buffered LED indicators
- Hard wired development area with access to all power
- Isolated RS-232C communications (115.2 Kbps max)
- 4 line X 20 character (blue) display with white LED
- In-circuit programming and debugging (RJ-12 connector)
- CCS PIC-C sample code and schematics provided (CD ROM)
- Operates from any battery or bench 6 to 12 VDC power supply
- Screw terminals for convenient wiring to external devices

RJL Systems has a 25 year history in medical devices and is proud to announce an analog development board for engineers and hobbyists who demand accurate signal processing for display and communications.

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33955 Harper Ave.
Clariant Twp, MI 48035
1-800-528-4513
www.realanalog.com

---

**Project**

**References**


C: > AVRASM -I LED1AVR.ASM LED1AVR.LST LED1AVR.HEX

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---

**About the Author**

G.Y. Xu is an electrical designer specializing in microprocessor/microcontroller systems design and development, both in hardware and software. He can be reached by Email at gyxu@cmpmail.com
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- 25mW and 1W models!

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- All new design, using SMT technology

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- Ideal for schools
- Microprocessor controlled
- Simple settings

Run your own radio station! The AM25 operates anywhere within the standard AM broadcast band, and is easily set to any clear channel in your area. It is widely used by schools - standard output is 100 mW, with range up to ¼ mile, but jumper settable for higher output where regulations allow. Broadcast frequency is easily set with dip-switches and is stable without drifting.

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Tunable FM Stereo Transmitter

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- Settable pre-emphasis 50 or 75 µSec for worldwide operation
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The FM10A has plenty of power and our manual goes into great detail outlining all the aspects of antennas, transmitting range and the FCC rules and regulations. Runs on internal 9V battery, external power from 5 to 15 VDC, or an optional 120 VAC adapter is also available. Includes matching case!

- Tunes the entire 550-1600 kHz AM band
- 100 mW output, operates on 9-12 VDC
- Line level input with RCA connector

A great first kit, and a really neat AM transmitter! Tunable throughout the entire AM broadcast band. 100 mW output for great range! One of the most popular kits for schools and scouts! Includes matching case for a finished look! The AM1 has been the leading Scouting project for years and years. Try out your kit skills and at the same time...get on the air!

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When we say "match" we mean electrical impedance match...if the proper impedances are not maintained between transmitter and antenna, power is reflected away from the antenna and back into the transmitter! This can cause the final amplifier stage to be damaged, not to mention spurious signals and lousy range. Don't forget, there are three important factors in your broadcast range: antenna, antenna, and antenna! Buy this kit and get the most from your FM Broadcast!

- Fully weatherproof-rugged PVC construction
- Matches 50 or 75 ohm systems
- Tunable for a perfect match over the entire 88-108 MHz FM band
- 25 watt RF power maximum

Our FM100B is the updated version of a truly professional frequency synthesized radio transmitter station in one durable, handsome cabinet. It is used all over the world by serious hobbyists as well as churches, drive-in theaters, and schools. No one else offers all of these features at this price! The included frequency display and audio level meters assist in easy operation. The "B" version now includes some additional functionality including a line level monitor output, improved stereo separation, spectral purity, audio clarity, and adjustable RF Output. An exclusive selectable microphone mixer and auto AGC circuit combines your local mic audio with your music input or mutes the music when mic audio is present. You don't even need an external mixer!

Sound quality is impressive; it rivals commercial stations. Low pass input filtering of the speakers puts maximum "pizzazz" in your audio, and prevent overmodulation distortion. No wonder everyone finds the FM100B to be the answer to their transmitting needs... you will too! The kit includes a sharp looking metal cabinet, whip antenna, and built in 110/220 volt AC power supply. An external antenna connection allows hook-up to high performance antennas like our TM100 and FMA200. We also offer a high power export version of the FM100B that's fully assembled with one watt of RF power for miles of program coverage. Many islands and villages use it as their local radio station! The export version can only be shipped outside the USA, or within the US if accompanied by a signed statement that the unit will be exported. (Note: The end user is responsible for complying with all FCC rules & regulations within the US, or any regulations of their respective governing body.)
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- DDS and SMT technology!
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SG560WT Audio/RF Signal Generator, Factory Assembled $329.95

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- 10MHz and 40MHz sample rates!
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HP510SE Personal Handheld 10MHz Digital Scope $229.95
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- RS232 output to your PC!
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Features both auto and manual ranging with a large 3½ digit display with a 38 segment analog bargraph. Selectable backlight and data display fold features are also included. Plug in the provided DB9 serial cable to your PC, load the included software, and you’re off and running with a remote control digital multimeter from your PC! Includes standard test probes, temperature test probes, professional rubber holster, RS232 cable, installed 9V battery, Windows software CD, all in a neat travel case. (Hard to believe for $85 isn’t it?)

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When I got my first computer in the early 80s, there was an immediate attraction. Hours and hours of playing turned into weeks and weeks, which turned into months and months. I was hooked. Once I had the language down, the first thing I wanted to do was write a game. For my first game, I thought big. It was going to be the game of games. I spent weeks writing the code on paper. (I didn’t have a storage device at the time, so I had to write my programs out completely and then type them into the computer in their entirety.)

Anyway, the day came when the program was done and I spent all night typing it in. At 2 o’clock in the morning, I was about 80% complete and my VIC-20 gave an out of memory error. I played the game as far as I could and it was still magical. The lesson to be learned was to write efficient code. That was not my last game or my last computer. That love affair has gone on for many, many years. I ended up in hardware with an electrical engineering degree, but I sometimes think about those old programming days.

Recently, while working on a project, the ezVID was created (by accident, of course). When I first saw the prototype of what was going to become the ezVID, I thought about some interesting possibilities. I have been using microcontrollers both personally and professionally for some time. One of the microcontrollers I like to play with is the BASIC Stamp 2. Could this new prototype be used with the BASIC Stamp 2? Could this be a microcontroller video card? Could the BASIC Stamp 2 handle game code and graphics? Could it be as fun as it was programming my first game into my first computer?

When the ezVID was completed, the final product sported a resolution of 188 x 254 with 14 different colors. There was a ton of custom character memory — 256 possible — which is needed for any good game or graphics program. To handle all the basic stuff — such as letters, numbers, punctuation, and basic symbols — the ezVID comes with a standard, built-in library of 63 characters. It has an asynchronous TTL level serial interface, power connections (+5 VDC and common that the user has to supply), and a standard RCA style jack for the video output. The video output is NTSC non-interlaced composite video and is compatible with any television, VCR, RF modulator, or any other piece of equipment that accepts this type of video input.

Where to Begin?

Now that it was all together, what game should be made first? It was obvious after a few moments of thinking that the answer has to be Pong. Pong looks about as basic as a game can get, but it does have a good handful of conditionals that have to be monitored and — if you really want to get serious — the laws of physics can be programmed into it to give the ball deflection vectors based on what angle it hits a wall or paddle.

For the BASIC Stamp 2 version, the laws of physics will have to be left out and only the conditionals will be looked at, along with ball speed increments, to make game play harder as you go.

To play games, it takes a little more than an ezVID and BASIC Stamp 2. The main ingredient that’s missing is a game controller. Every game you play has some form of user input, whether it is a
game paddle, joystick, or just a few buttons. For Pong, the interface of choice is a paddle. The complete schematic, including the paddle, is shown in Figure 1. The game paddle for this system has to be made. This is an easy job that requires only a 1K ohm potentiometer, SPST normally open momentary switch, enclosure, knob, and a cable to connect it to the BASIC Stamp 2. Refer to the photo of a sample paddle in Figure 2. However you build your paddle, make sure that it is wired so that a clockwise rotation increases the resistance between the two terminals you are using and a counter-clockwise rotation decreases the resistance.

Once you have your paddles completed, you can assemble the hardware. Following the schematic in Figure 1 and the Parts List, you can build your proto-board very easily. The proto-board does not have the interface for the BASIC Stamp 2 to communicate with the PC, so you will have to download your BASIC Stamp 2 code prior to placing it in the Stamp Pong proto-board. A picture of a completed Stamp Pong proto-board is shown in Figure 3.

### Getting Started

Before you can start writing any exciting game code, we must first explore the basics. In this case, that is communicating with the outside world which is the ezVID and the game paddle. Once this code is in place and working you can make them into subroutines and call them whenever needed in your code.

Let’s first take a look at the ezVID and its commands. It is important to note that, for these examples, it is assumed that P14 of the BASIC Stamp 2 is connected to pin 2 of the ezVID and P15 of the BASIC Stamp 2 is connected to pin 3 of the ezVID, as in the schematic in Figure 1. In the sample code, you will see that SEROUT is the main command used and it is set up to send data through pin P15 at 9600 baud (non-inverted) with a 1 mS pause between each byte of data. The 1 mS pause in the command is used to adhere to the ezVID timing characteristics. When you send the ezVID a byte of data, you must first wait for an acknowledgment (ACK) return before you send another one. If you send another byte before receiving the ACK, the data will be lost.

The manual for the ezVID states that the ACK will be returned a minimum of 139.68 nS to a maximum of 663.56 µS after the stop bit of the data packet being sent is received. Putting the 1 mS delay between each byte ensures that enough time has passed for the ezVID to receive the byte of data and start sending its ACK before sending another one. PAUSE 1 usually follows SEROUT (except change background color, clear screen, and reset). This is to allow enough time for the ezVID to ACK the last byte sent.

The last command normally used, PULSIN, is a way to tell that the ezVID is ready for another command (not needed when changing background color, clearing the screen, or resetting). Once the last byte is ACKed by the...
Project

adding a custom character

This sample code defines a lower case “e.” The SEROUT command sends 65, which is the code for adding a user-defined character. The next byte is 0, which is the character number assigned to the lower case “e,” which can be from 0-255. The remaining 14 bytes are the bitmap information that makes up the character:

```
SEROUT 15,84,1,[65,0,0,0,0,0,24,60,102,66,126,126,64,13,0]
PAUSE 1
PULSIN 14,0,RS_IN
or
SEROUT 15,84,1,[65,0,0,0,0,0,24,60,102,66,126,126,64,13,0]
PAUSE 17
```

change background color

The SEROUT command sends 66, which is the code for change background color along with a color (0-13) — 13, in this case, for orange. PAUSE 4300 waits for 4.3 seconds, the time it takes to change the entire background color before the e2VID sends the READY response:

```
SEROUT 15,84,1,[66,13]
PAUSE 4300
```

clearing the screen

The SEROUT command sends 83, which is the code for clear screen along with a color (0-13); here, we use 0 for black. PAUSE 1600 waits for 1.6 seconds, the time it takes to clear the entire screen before the e2VID sends the READY response:

```
SEROUT 15,84,1,[83,0]
```

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A2VID, you have to wait for it to complete that command before sending another one. The e2VID will send a READY when it has completed the command. If another command is sent before the READY, then the e2VID will throw it out and reset the receiver when it sends the READY.

The e2VID manual states that the time required to complete most commands is a minimum of 663.56 μs and 16.62, mS maximum (except to change background color and clear screen). It has been found that, if the e2VID responded quickly (around the minimum of 663.56 μs), part of the READY byte will start sending before the BASIC Stamp 2 can start executing a SERIN command, so it couldn’t be used. The obvious solution is to put in a 17 mS delay to wait out the maximum time before sending more commands.

This method has a pro and a con; it takes up less space in the BASIC Stamp 2, but takes longer to execute. The PULSIN command works well and keeps the program moving along. The reason it executes more quickly is that you usually do not have to wait the maximum time for the e2VID to start sending the READY response. By the time the PAUSE 1 command is completed and the BASIC Stamp 2 starts the PULSIN command, the ACK from the last byte sent is already done and the serial Tx line from the e2VID is being held high, waiting to send its READY or it just started sending READY.

Since the serial Tx line from the e2VID is going to toggle between high and low while it is sending READY, the PULSIN command is the perfect choice. When READY is sent from the e2VID, the PULSIN times the pulse of the first low state it sees and then returns it in the variable RS_IN. You don’t care about the value in RS_IN, but — since the PULSIN command is complete — that means the e2VID is sending READY, since a high-to-low and low-to-high transition was seen. This gives a quick response time while adhering to the timing characteristics of the e2VID. Since RS_IN is not used, make it a Bit size so space in RAM is not wasted.

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PAUSE 1600

**Drawing a Character**

The SEROUT command sends five bytes: COMMAND, CHARACTER, COLOR, XPOS, and YPOS. COMMAND defines whether the ezVID is going to place a built-in or user-defined character: COMMAND=67 for a built-in character and 85 for a user-defined character. CHARACTER tells the ezVID which character to place: 0-62 for built-in characters and 0-255 for user-defined characters. COLOR tells the ezVID which color to place it in: use 0-13. XPOS is the X-axis position to place the character in: use 1-188. YPOS is the Y-axis position to place the character in: use 1-254:

```
SEROUT 15,84,1,[COMMAND, CHARACTER, COLOR, XPOS, YPOS]
```

**Reset ezVID**

The SEROUT command sends 82, the code for resetting the ezVID. Once you send reset, wait for 250 mS for initialization to be complete:

```
SEROUT 15,84,[82]
PAUSE 250
```

Drawing a character is the most common thing you will do in all your programs. In Stamp Pong, this is a subroutine. The main code sets up the variables and then the routine is called to communicate with the ezVID. This saves a lot of code space and time.

The game paddle is the user interface. Refer to Figure 1, which shows the paddle interface to the BASIC Stamp 2. The paddle is connected to pins P0 and P1. The paddle works very simply. The fire/select button is connected to pin P0. This line is held high logic by a pull-up resistor, R1. The fire/select button is a momentary SPST normally open push-button connected to ground. When the fire/select button is pressed, the pin will be pulled logic low. To read the fire/select button, you use the following command:

```
IF IN0=0 THEN {insert label you want the program to goto here}
```
The variable “PADDLE” is equal to 134. If you hold the paddle for example, you move the paddle to a location where the RCTIME command returns a different value for each read. Caused when the paddle is not being moved, but the capacitor and 1K ohm potentiometer was chosen so the RCTIME command will return as close to a single byte number (0-255) as possible on the BASIC Stamp 2.

The first two commands, HIGH 1 and PAUSE 1, turn pin P1 into an output logic-high pin for 1 mS. This discharges the capacitor before executing RCTIME. When RCTIME is executed, pin P1 is turned into an input and capacitor C1 will start to charge up through the potentiometer in the paddle. When pin P1 turns from a logic high state to a logic low state, the value is stored in the variable “PADDLE.” The combination of the 0.47 µF capacitor and 1K ohm potentiometer was chosen so the command would execute quickly; the less time the command waited for the capacitor to charge, the faster the game play could be. They were also chosen so the RCTIME command will return as close to a single byte number (0-255) as possible on the BASIC Stamp 2.

Paddle jitter may occur in your programs. Jitter is caused when the paddle is not being moved, but the RCTIME command returns a different value for each read. For example, you move the paddle to a location where the variable “PADDLE” is equal to 134. If you hold the paddle at that point and constantly execute the RCTIME command, you will notice that — most of the time — a value of 134 will be returned, but values of 133 and 135 will also be returned on occasion.

You can reduce this with hardware changes, such as better tolerance components and high precision potentiometers. You can also reduce it with software, such as reading the paddle 10 times and then taking the average value. You can experiment with this in Stamp Pong. Resistor R2 completes the paddle circuit. This is simply protection against short circuits. When the capacitor is completely charged up, the negative side is at 0 volts. Executing the HIGH 1 command would cause an instantaneous in-rush current to occur during the discharge. This resistor is just some insurance to keep the BASIC Stamp 2 from experiencing high in-rush currents.

### Gaming Code

The interface and communications stuff is out of the way, so let’s get on to the real stuff. When the game first executes the variables and the initial pin settings are done, the program will wait to make sure enough time has passed for the ezVID to initialize itself, send the command to clear the screen, and then begin loading custom characters. The custom characters are an off light bulb, an on light bulb, a brick piece, and the ball.

The main game code is then executed. The game is broken up into three pieces: the title screen, the paddle color selection screen, and the main game screen. These are shown in Figures 4 through 6, respectively. The title screen is shown first and is also the screen that the game returns to when the game is over. It is simply the name of the game “STAMP PONG” surrounded by a constantly rotating light show. Instructions appear to prompt the game player to press the fire button when ready. This code is a tight loop where the BASIC Stamp 2 is constantly sending commands to the ezVID to place a “light on” character, place a “light off” character in the same position, increment the position, and check to see if the fire/select button on the paddle has been pressed. As long as the fire/select button has not been pressed, the rotating light show will continue to go around the game title.

When the fire/select button is pressed, the title screen is cleared and the paddle color selection screen is drawn. Here, the user can select the color of the paddle in the game. This is the first instance where the code to read the paddle is used.

The value of “PADDLE” is used to determine the position of the arrow. Two conditions are checked; if the value of PADDLE is greater than or less than the selection...
area, then the value is ignored and the last value is used. When the user presses the fire/select button, the position of the selection arrow is noted and the paddle color is written into the variable “PADDLE_COLOR.”

Once the paddle color has been selected, the screen is cleared and the main game screen is drawn. This version of Pong is made for a single player, so a brick wall is drawn along the top and bottom, as well as along the right side of the screen. The paddle is placed on the left side of the screen and the score is located in the upper left-hand corner. Game play is simple: hit the ball back into the playing field when it comes to you. Every time you hit the ball, the score is incremented by one. For every five points you score, the ball speed is increased by one; the longer you play, the faster it gets. The first time you miss the ball, the game ends and “GAME OVER” appears in the center of the screen. In five seconds, the screen will clear and the title screen re-appears.

Stamp Pong has very simple collision detection; you have to check the walls and the paddle and that’s it. The walls are simple; they don’t move. You know where they are at all times, so their value is constant. Every time you move the ball, you check to see if the new position is beyond one of those constants. If it is, then draw the ball just touching the wall and change its direction. Even the paddle is pretty simple. The X position never changes and you know the Y position from your paddle read that is stored in the “PADDLE” variable. Treat the paddle just like a wall. If the new ball position is going to cross the X boundary of the paddle, then check the Y position. If the ball hit the paddle, redraw the ball just touching the paddle and change its direction. If it didn’t hit the paddle, then the game is over.

When changing the direction of the ball, you just have to know its last direction and what it hit. If the ball is traveling up and it hits the top wall, then change its traveling direction to down. However, if a ball is traveling up and it hits the back wall, you don’t change its Y-axis direction, but rather its X-axis direction — which is left and right. Since the ball hit the back wall, if it was traveling right, you would change its direction to left.

There is one last conditional that you need to check: the paddle position. As mentioned before, the RCTIME command will return a value of approximately 0 to 255 for the complete travel of the potentiometer in the user paddle. The paddle on the screen — just like the ball — has to be confined within the walls. Each time RCTIME is read, the Y position is checked to see if the new position will be outside one of the walls. If it is, then the new value is thrown out and the previous paddle position is used instead.

**Conclusion**

A lot has been done since the ezVID was created and Stamp Pong was made to try it out. New games and drawing programs have been made and they get better all the time. Every time a program is made, new possibilities are thought up and more is learned.

Well, that’s all for now. You’ve been presented with the basics of hardware and software for gaming and graphics with the ezVID and the BASIC Stamp 2. The rest of it is up to you. Remember: Be creative. Optimize your code so you can do more with less. Keep in mind the limitations of your hardware, but don’t let this limit your imagination. Get a clear picture of what you are going to do first and how best to achieve it by looking at all your possibilities. If you’re going to make a game, get all the rules together first so you can code them in. Most important of all — have fun!

In front of me is a BASIC Stamp 2 and an ezVID, but in my mind, I’m back programming games on my old computer ... **NV**
**NEW 1,000 A AND 800 A CLAMP METER SERIES**

Extech Instruments announced its new series of 1,000 A and 800 A clamp meters. Each 1,000 A clamp features a unique, built-in, non-contact Infrared thermometer with a laser pointer to monitor temperature and locate hot spots on motors and electrical devices. Each 1,000 A meter features min/max, a data hold feature that "freezes" the data in the display, and an auto ranging feature with a manual range override.

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Rabbit Semiconductor has introduced the Multi-Port Serial-to-Ethernet Kit. Rabbit Application Kits enable embedded designers to quickly implement common application needs without designing from scratch. The Multi-Port Serial-to-Ethernet Kit allows multiple ports to convert data from serial to ethernet. In addition, this new kit allows bi-directional conversion — from serial-to-ethernet and ethernet-to-serial.

Serial-to-ethernet conversion is necessary for data to be remotely monitored via most networks or the Internet. The Rabbit Multi-Port Serial-to-Ethernet Kit provides the hardware and software necessary for sensors and other serial devices to communicate via a LAN or other network. Implementation of the optional RabbitWeb software module makes it simple to web-enable applications to allow monitoring and control of serial devices via the Internet or Intranet.

Other optional software modules help secure data through SSL and encryption.

The Rabbit Serial-to-Ethernet Kit uses a temperature sensor application to guide users through serial-to-ethernet conversion. Based on the RCM3700 RabbitCore, the kit also includes a prototyping board, the Dynamic C development environment with a royalty-free TCP/IP stack and source code, sample applications, a temperature sensor for the sample application, required cables, and assorted accessories. The sample applications highlight functionality, such as RS-232 to ethernet conversion, RS-485 to ethernet conversion, ethernet-to-serial conversion, data gathering from serial devices — such as the included temperature sensor or...
digital voltmeter (which is not included), and web-enabling applications.

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**FREESCALE ZIGBEE™ WIRELESS TECHNOLOGY**

MaxStream, Inc., has adopted the Freescale Semiconductor, Inc., platform for an assortment of ZigBee™ wireless products. MaxStream will shortly introduce the Federal Communications Commission and CE-type approved XBee™ family, which incorporates Freescale’s ZigBee-ready and 802.15.4 chipsets onto MaxStream’s RF modules. The XBee line of RF modules and stand-alone connectivity solutions will allow OEMs to add wireless capabilities to their products easily and quickly. The ZigBee wireless standard is a cost-effective solution for connecting electronic devices in a short range wireless mesh network.

MaxStream will offer two versions of the XBee ZigBee module, allowing OEMs the choice between either low cost or high performance modules. The low cost XBee module measures less than one square inch, while the 100 mW high performance XBee-PRO™ module is only two-thirds of an inch larger and achieves up to three times the range of standard ZigBee modules. Both module designs are network and form-factor interchangeable, allowing the modules to be easily upgraded or reconfigured to meet the changing needs of each ZigBee network. RS-232, USB, and ethernet interfaces will also be available in 2005, creating simple connectivity solutions to computers and other electronic devices.

Additional ZigBee-based products — including a wireless bridge that permits ZigBee networks to connect to long-range MaxStream radios — will be made available to complement the capabilities of both ZigBee and MaxStream proprietary networks.

Freescale’s ZigBee-enabled platform includes the MC13193 2.4 GHz RF chip, a low voltage, low power HCS08 MCU, and the Z-Stack ZigBee software for a robust, cost-effective, and easy-to-deploy solution. The MC13193 on-chip features and enhancements reduce external components and total bill of materials cost while providing battery type flexibility with lifetimes of up to several years.

The XBee module operates in the 2.4 GHz ISM bandwidth and will come with the necessary software to create ad-hoc ZigBee networks. The modules are designed to transmit at power-efficient levels and power-down sleep modes help conserve additional energy when data transmission is intermittent.

MaxStream offers unlimited free technical support for all of its wireless technology via telephone, Email, and online chat, making it easy for customers to integrate ZigBee technology into each specific design.

For more information, contact:

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An Engineer’s Engine

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To download the Engineering Toolbar, go to www.globalspec.com/Engineering-Toolbar/install. At present, you’ll need MS Windows 98, Me, NT, 2000, or XP and Internet Explorer 5.0 or newer.

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CONFIDENTLY USING INTERRUPTS IN YOUR MICROCONTROLLER PROJECT

by Phil Mass

Why Use Interrupts?

Interrupts are very powerful tools built into almost every microcontroller. If you write microcontroller code, I can guarantee that they will make your life easier. Once you learn the basics of interrupts, you will find that they work essentially the same on all microcontrollers.

If you’re planning on counting instructions or adding NOPs to your code to get precise timing, you’ll need to learn about interrupts. You’ll find that they not only make it easier to write your code the first time, but — when you have to change the timing of your project — they will really save you time and headaches. Instead of recounting all those instructions, you can just change the interrupt timing by changing a single constant.

If you need to do anything in real time — like controlling a motor or generating and reading communication signals, such as serial streams — interrupts are the way to go. With an interrupt, you will be assured that the timing of your signals will be right. Without consistent timing, you can get jerking in your motors and hard-to-diagnose errors in your communication routines.

Once you’ve become familiar with using interrupts, they will become like the heartbeat of your code, the regular rhythm at the core of your project. You’ll find that they aren’t intimidating and you’ll wonder how you ever wrote microcontroller code without them. You will start designing your project around the interrupt and find that this simplifies the design and makes development faster.
What Is an Interrupt

If you don’t use interrupts, I hope that I’ve motivated you to learn more about them. Let’s start by defining an interrupt. Although there are many different types of interrupts, in this article I will only discuss periodic timer-generated interrupts because I’ve found them to be the most useful; they are also available on almost any microcontroller. Once you’ve learned about timer interrupts, though, it will be easy to extend the basic concepts to other types of interrupts.

In the case of a timer-generated interrupt, the interrupt is an event in the microcontroller that lets you run a short section of your code at a regular interval. For instance, you might set up an interrupt to run at 1 kHz — or 1,000 times per second. In this case, every one thousandth of a second, you will get an interrupt. Like the ticking of a sped-up clock, the interrupts occur on a set schedule and they occur no matter what else is going on in the main body of your microcontroller code.

Each time the interrupt occurs, the microcontroller will run and interrupt is enabled, this rollover will generate an interrupt. When a timer reaches its maximum value (255 for an eight-bit timer), it rolls over to a value of 0. If your timer interrupt is enabled, this rollover will generate an interrupt.

For eight-bit microcontrollers, timers that can generate interrupts are usually eight bits or 16 bits, sometimes with prescalers to extend their ranges. A prescaler allows you to get slower interrupt rates with an eight-bit timer, though with less precision. For instance, a prescaler value of 4 tells the microcontroller to increment the timer every fourth instruction cycle instead of every cycle, so that your interrupt frequency is a fourth as fast.

What exactly does it mean to generate an interrupt? To understand this, you need to know what is normally happening when a microcontroller is running. When you program a microcontroller, you place the assembly instructions of your code into sequential program memory addresses. In the simplest case, a microcontroller performs the instructions in its program memory in order. If it just performed the instruction at address location 123, then it will run the instruction at location 124 next.

However, when an interrupt is generated, the microcontroller jumps to a fixed interrupt address instead of going to the next instruction. This special address is sometimes called the interrupt vector and is often toward the beginning of the program memory. This location is where you put the start of your interrupt code. So, generating an interrupt really means making your microcontroller jump to a known address — the start of your interrupt routine.

When the interrupt has done its work, you want the microprocessor to go back to whatever it was doing just before the interrupt happened. There is a special return-from-interrupt instruction that does just this. It signals that the interrupt processing is over and that the microcontroller should go back to where it was prior to the interrupt.

One thing to keep in mind when using an interrupt is that you don’t want to overwrite variables you were using in your main code. This is especially true of the accumulator or working register and any status flags. Some microcontrollers will store some of these important variables for you automatically and restore them at the end of the interrupt. If you are using a compiler, it will usually do this for you if

How an Interrupt Works

Microcontrollers have special hardware built into them to generate and handle interrupts. In the case of a timer-generated interrupt, the microcontroller generates an interrupt whenever a specific timer rolls over. Almost all microcontrollers have timers; timers are built-in register variables that are incremented every instruction cycle. Counting the instruction cycles is the same as counting the time. Certain instructions take more than one instruction cycle to run, but the instruction cycle time is constant. When a timer reaches its maximum value (255 for an eight-bit timer), it rolls over to a value of 0. If your timer interrupt is enabled, this rollover will generate an interrupt.

FIGURE 1. An oscilloscope trace of a typical interrupt.
the microcontroller doesn’t, but — if you are writing assembly code directly — you will want to copy the value of the accumulator and any processor flag registers into temporary variables at the start of your ISR and then copy those values back into the registers at the end of the ISR just before the return-from-interrupt instruction.

To recap, the whole process happens as follows: Your microprocessor is performing instructions in the main body of your code. As this is happening, the timer is incrementing. When the timer rolls over from its maximum value to 0, the microcontroller jumps to the interrupt vector address in its program memory. It runs through the instructions of your interrupt routine until it reaches the return-from-interrupt instruction. It then jumps back to wherever it was when the interrupt was generated and keeps running.

Different microcontrollers can also generate interrupts under other specific conditions. For instance, many microcontrollers have special external interrupt pins or pins that can generate interrupts when their state changes. These interrupts operate in much the same way, apart from their triggering. The interrupt service routines will have the same parts, except that they won’t need to reset the timer. When you are using more than one source to generate interrupts, you will need to check which source generated each interrupt at the beginning of your interrupt routine.

The Details — Setting Up and Using Interrupts

There are several things you need to do to get a periodic interrupt running on your microprocessor. I’ll talk about them in general and also give the specifics of getting a periodic interrupt running on the popular Microchip PIC16F84 processor clocked at 10 MHz. The PIC16F84 processor can be purchased from Digi-Key (www.digikey.com).

First, you will need to decide on the frequency of your interrupt. You will choose your interrupt frequency depending on the needs of your application. For our example, we will use the interrupt to generate a 255 step PWM signal on an I/O pin at 200 Hz to control a motor. Since we’ll need an interrupt for each step of the PWM, we’ll need 255 interrupts every 200 Hz, giving us a desired interrupt frequency of 51,000 Hz (200 Hz * 255 = 51,000 Hz).

Next, we need to figure out how many times the timer will increment between interrupts. To do this, we divide the frequency of the timer by our desired interrupt frequency. From the data sheet...
for the PIC16F84, we know that Timer0 — which is used to generate interrupts — increments once every instruction cycle (not using the prescaler). Also from the data sheet, we know that there is one instruction cycle for every four clock cycles, giving us an instruction cycle frequency of 2.5 MHz (10 MHz / 4 = 2.5 MHz). We now divide this by our desired interrupt frequency of 51,000 and we get 49.02 (2,500,000 / 51,000 = 49.02). Since we need an integer number of timer increments per interrupt, we round this to 49. So, the timer will increment 49 times from one interrupt to the next.

Now, the next fact we need to know is that Timer0 causes an interrupt when it rolls over, when its value goes from 255 to 0 (255 is the maximum value for an eight-bit timer). From the last step in our calculation, we know that we want 49 increments between interrupts to get our desired frequency. So, if we subtract 49 from the timer’s value during our interrupt, we know that the next interrupt will occur 49 cycles later than this one. This is how we set the interrupt frequency. If we don’t change the timer’s value during the interrupt, we will instead get interrupts every 256 cycles when the timer naturally rolls over.

Another thing to keep in mind is that you might have to adjust the value you subtract from the timer because you lose a few cycles doing the subtraction. This is because the timer value will continue to increment while you are doing the subtraction. For instance, if reading the timer, subtracting, and writing the timer again takes three cycles, you will want to actually subtract 46 from the timer instead of 49. Otherwise, your interrupt frequency will be slightly off.

An alternate way to set the interrupt frequency is to load a constant value into the timer at the beginning of each interrupt. This method uses fewer instructions to set the timer, but is less accurate because it doesn’t take into account the interrupt latency. The interrupt latency is the few instruction cycles it takes between the timer rolling over and the first instruction of your interrupt service routine. The interrupt latency varies for different microcontrollers and can also vary slightly from interrupt to interrupt, depending on the microcontroller. When the latency varies slightly, so will your interrupt frequency.

If we were to use this method in our example, what value would we need to load into the timer at the beginning of our interrupt so that — 49 cycles later — the timer will roll over? We subtract 49 from 256 (the timer rolls over one cycle after it reaches 255) and get an answer of 207. So, if we load a value of 207 into the timer at the beginning of our interrupt, the next interrupt will happen when the timer rolls over 49 cycles later. If you really need to make your interrupt routine short, this can be a good alternate way to set the interrupt rate.
**CONFIDENTLY USING INTERRUPTS IN YOUR MICROCONTROLLER PROJECT**

Microcontrollers signal that an interrupt condition has been reached by setting a flag — a bit in one of the system registers. For our timer interrupt, this flag is set when the timer rolls over. If that interrupt is enabled, this will trigger an actual interrupt. In most microcontrollers, you will need to clear this flag by hand in your interrupt routine or you will keep getting the same interrupt over and over. For our Timer0 interrupt in the PIC16F84, this means clearing the T0IF bit with a BCF instruction.

The next step is writing your actual interrupt service routine. You already know a few things that need to appear in the routine. At the beginning, you need to save the state of important registers, clear the flag, and subtract your interrupt cycle value from the timer. At the end of the interrupt, you need to restore the register values you saved and then have a return-from-interrupt instruction. The return-from-interrupt instruction is always the last instruction of your interrupt service routine.

Here are the tasks that you will need to do in each of your interrupt service routines (See the interrupt service routine in the sidebar for a specific example.):

1. Save the values of the system registers you use in the interrupt.
2. Subtract from the timer the “timer increments per interrupt” value you calculated.
3. Clear the interrupt flag.
4. Write the body of your interrupt. In our example, this is the PWM generation code.
5. Restore the system register values that you saved.
6. End your interrupt routine with the return-from-interrupt instruction.

The final step to getting your interrupt running is to set the hardware bits that enable the interrupt and the timer. Most microcontrollers have both a global interrupt enable bit and bits that enable each individual type of interrupt. When the global interrupt enable bit is not set, all interrupts in the microcontroller are disabled. For an interrupt to be enabled, both the global and the individual interrupt enable bits must be set.

In the PIC16F84, you can set these bits directly using the BSF instruction. The global interrupt enable bit is named GIE and the Timer0 interrupt enable bit is named T0IE. You also need to set up and enable the timer so that it starts incrementing every instruction cycle. In my example, I set the PSA bit to have no prescaler and set the T0CS bit to start the timer incrementing. You only need to set these values once, unless you want to turn the interrupts on and off. I usually set them in an initialization section at the beginning of my main body of code.

If you are writing your interrupt routines in a C compiler, the compiler may take care of some of these details for you. It will probably enable you to write the body of your interrupt routine in a special interrupt function. From this function, it will generate the assembly code and place the routine at the correct interrupt vector address and also save the state variables for you. Some microcontrollers also automatically save the important registers for you whenever an interrupt occurs and then restore them when the interrupt is over. Refer to your microcontroller’s data sheet to see if it saves any register values automatically.

One general rule to remember is to keep your interrupt code short. This is a solid principle, but it doesn’t mean that you can’t do any processing in your interrupt. The thing you want to absolutely avoid is for the next interrupt to occur when the last one is still running. In our example, we generate an interrupt every 49 instruction cycles. So, it’s clear to see that — if our interrupt routine takes more than 49 instructions to run — the next interrupt will want to run before the current one is over. This is a problem and it means that the main body of your code will never get to run.

The longer your interrupt routine, the less processing time is left for your main code. Because of branches in your code, the number of instruction cycles it takes to run can vary from interrupt to interrupt. In practice, I’ve found that interrupt routines can take up 50% of the time between interrupts without causing problems. In our example, this would mean an interrupt routine that runs in 24 instructions or less. Overall, shorter is usually better.
How to Know It’s Working

Now that you’ve done writing your interrupt code, how do you confirm that you did everything right? It is really easy to debug an interrupt if you have an oscilloscope. Add two more instructions to the main body of your interrupt routine. At the very beginning of the body, set one of your microcontroller pins high. On the PIC16F84, you can use the BSF and BCF instructions to set just one pin at a time. At the end of the interrupt body, set the same pin low. Then, run your application and hook an oscilloscope to the pin. You should see an oscilloscope trace like the one shown in Figure 1. The time from the beginning of one pulse to the next is the period of your interrupt. The width of each pulse divided by the period gives you the approximate percentage of processing time that your interrupt is using. Keep in mind that this doesn’t take into account the latency or the setup and ending instructions. The real time taken by the interrupt is a bit more.

If you don’t have an oscilloscope, there are still easy ways to check that your interrupts are running and at the right frequency. A good debugging tool is an LED hooked up to one of your microcontroller pins. If you did what I explained above, the LED would blink, but it would blink so fast that you would never be able to see it. So, you need to slow down the blinking by incrementing a counter. In our example, the interrupt rate is 51,000 Hz. If we divide the frequency down by 51,000, our LED will blink on for a second and then off for a second. We can use two cascading eight-bit timers or one 16-bit timer to accomplish this. For the eight-bit case, you would increment your first timer in each interrupt. Whenever this timer rolled over (from 255 to 0), you would increment your second timer. When the second timer reached 200, you would set it back to 0 and flip the state of your pin from high to low or low to high. In this way, you can confirm that your interrupt is running and running at the right rate because the LED is blinking on for a second and then off for a second.

Once you have your first interrupt running, you will know all the basics of using interrupts. These same methods will work on any microcontroller, with slight changes to handle the specifics of the hardware. As you become comfortable using interrupts, you will start to find more uses for them in all of your microcontroller projects.

About the Author

Phil Mass developed all of the software in the original Roomba robot vacuum cleaner while at iRobot Corp. He now has his own company, Element Products, Inc. (www.elementinc.com), specializing in product development consulting. He can be reached at pmass@elementinc.com.
In Part 1, we laid the foundation for the Proportional Integral Derivative PID controller. Using a simple, intuitive approach, we explored what each term represents. We examined how simple op-amp circuits could be used to construct the individual elements. In Part 2, we will see a complete analog PID system. We will explore the dynamic operation of the PID control system. We will explore how to operate and tune a PID controller. Using our servo motor example, we will explore system stability. We will learn new terms, such as overshoot, dampening, and oscillation. We will see how the individual P, I, and D terms come together to form a complete control system.

Last month, we came to several conclusions about each of the P, I, and D terms. These concepts are very important to our present discussion, so we will review them again. You can follow along with the block diagram shown in Figure 1.

**Proportional Concepts (PRO)**

A system will try to correct the error between the set point and the measured output. It does this by commanding the system in a direction that opposes the error. The intensity of the correction is determined by proportional gain. The proportional component provides a correction only if there is an error!

**Integral Concepts (INT)**

The integral section operates when an error is present. It accumulates this error over time. Therefore, a small error can become a large correction, given enough time. As the error is accumulated, the system will be forced to correct the error. Finally, the integrator will overshoot the set point. An error opposite of the original is required to discharge the capacitor.

**Derivative Concepts (DIF)**

The output of the differentiator is proportional to the speed of the system. If the system is moving fast, the output...
is high and vice versa. If the motor is not moving, the
differential output will be zero. The differential term is
applied in such a way as to slow down the motor.

**Circuitry**

A simplified schematic for the PID controller was printed
in Part 1. A new, more advanced, schematic is presented
here as Schematic 1. A new circuit has been added
consisting of IC3A, IC3B, and IC1. Again, this circuit is an
adaptation of the PID controller presented by Professor

This new circuit is designed to prevent the integrator
circuit from functioning under certain conditions. The
reasons for this added feature will be explained later in this
article. The analog switch (Maxim MAX318) disables the
integrator by shorting the integrator’s input to ground. The
analog switch is driven by op-amps IC3A and IC3B. This
pair of op-amps forms what is commonly called a window
detector. The name refers to the “window” of voltage where
the op-amps have a low output (allow the integrator to
function). If the output of the PID controller is above or
below a certain point, the op-amps will turn on the analog
switch, thereby disabling the integrator.

**Construction**

The circuit board shown in Photo 1 was designed for
this article. You can download the CAD files (Eagle) from
the Nuts & Volts website at [www.nutsvolts.com](http://www.nutsvolts.com) The CAD
file is slightly different than the board shown here. I made a
few minor modifications/improvements to the board. Feel
free to use the CAD files as you see fit. In case you were
wondering, Advanced Circuits manufactured this board. I
am very happy with their service. Check out their website at
[www.4pcb.com](http://www.4pcb.com) — look for their bare bones special.

As an alternative to the PCB, you could construct the
circuit using “dead bug” or perfboard construction. The
layout isn’t critical. I was able to breadboard this circuit
successfully. Just remember to keep the wire runs short
and decouple the op-amps.

**What Are We Controlling?**

We will be controlling the position of a servo motor. Our
servo motor is a mechanical device. Yes, this is an obvious

![Schematic 1. The advanced PID controller schematic.](image-url)
statement, but take a moment to think about the attributes of a mechanical system. The moving parts of a motor have mass. Consequently, they have inertia and momentum. It takes a finite amount of time before the motor will respond. It takes time and energy to get the motor armature, gears, and load moving. Figure 2 shows how the modified HiTec HS-322 R/C servo motor responds when a 6 VDC signal is applied. We see that it takes approximately 20 mS before the motor even starts to move. Conversely, once the motor is moving, it does not want to slow down.

The motor is also an electrical device — again an obvious statement. The motor windings have the characteristics of an inductor and a resistor. Recall that an inductor works to keep the current constant. Consequently, when the motor is turned off, there is no current flow. When the voltage is first applied, the inductance of the windings tries to keep the current at zero. Therefore, the motor inductance accounts for some of the delay seen in Figure 2. The motor resistance also limits the amount of current and, thus, the torque that the motor can deliver.

**How Do I Connect the Servo Motor?**

In a word, carefully! Things can get out of control when designing and experimenting with control systems. In preparing this article, I stripped no less than three sets of gears out of the servo motors! After that, I got smart and added limit switches to the servo. Also, it is a good idea to put a current-limiting resistor in series with the motor — 10 to 20 ohms works nicely.

The PID loop requires negative feedback. If either the motor or feedback resistor is installed incorrectly, we will have positive feedback and the system will go nuts. Remember those limit switches!

When we first connect the PID, it is best to disable the integrator and differentiator. The integrator is disabled by shorting out the feedback capacitor. The differentiator is disabled by shorting out the resistor connected between IC3D and ground. These components are marked on Schematic 1. On my circuit board, I have added headers to facilitate this process. Just add a shunt on top of the headers to disable the integrator’s derivative section.

The motor and feedback resistor should be connected to the circuit. If possible, do not physically connect the motor shaft to the feedback resistor. If you are using a servo, the top may be opened and the final gear removed. Short the set point, i.e., 0 volts input. Apply power to the system. The motor will most likely turn. Move the feedback resistor. You should be able to make the motor change directions. The motor should turn in a direction opposite that of the feedback resistor. If it doesn’t, reverse the polarity of the motor.

At this point, we can physically connect the motor and the feedback resistor. Be ready to disconnect the power. Things can get out of hand quickly. When power is
applied, the motor will either move the feedback resistor to midrange or the system will oscillate back and forth. If the system oscillates, decrease the proportional gain.

**How Do I Tune a PID Controller?**

This question is a bit like asking how to ride a bike. The best answer is to just do it. I chose the servo motor example as the basis of this article because it operates at just the right speed. The system is slow enough so that we can see what is happening, but not so slow that we have to wait to see our changes. This is nice because we can quickly tune the system. Taking this analogy further — tuning a PID controller is like riding a bicycle. We are trying to balance three criteria, as shown in Figure 3. An ideal system would be unconditionally stable. It would respond instantaneously to an input and it would have no error, i.e., it would go exactly where we tell it to.

There is no such thing as an ideal system and our servo motor is no exception. We already know that the servo motor is a slow device. It takes over 20 mS before the motor starts moving. We also know that it will not stop instantaneously. Once it is moving, the momentum will keep it moving.

In real systems, we are left with compromises. We are left to balance stability, rise time, and steady state error. Let me explain using a series of oscilloscope views. The test set-up used to capture the “oscillographs” is shown in Photo 2. In the following sections, we will observe the “step response” of the servo motor system.

A step input is nothing more than a square wave. We are telling the servo motor to instantly move from one position to another. The blue line represents the step function applied to the input. The red line represents the actual response of the servo mechanism, as measured at the feedback resistor.

**Proportional Control**

We will first examine how the servo motor responds to changes in proportional gain. The integrator and differentiator should be disabled at this time. When we adjust the proportional gain, we are adjusting how hard the system will be driven. Higher proportional gains send more current to the motor. The motor will develop more torque and, as a result, will move faster. This results in a more responsive system that is better able to follow the set point. However, there is a limit, as can be seen in Figure 4. The curve in Figure 4 is a classic example of an “under damped” system. In an under damped system, the system is seen to oscillate about the set point in response to a step input. The system is optimized for rise time. The final steady state error is minimal.

In Figure 5, we see what happens when the proportional
THE PID CONTROLLER — Part 2

gain is lowered. This figure shows a classic "critically damped" system. The response is as fast as possible without overshoot. If the gain was increased, the system would overshoot and oscillate, as seen in Figure 4. If the gain was lowered, the system would be "over damped" and would take even longer to arrive at the set point.

The critically damped system is optimized for stability. The risetime performance has decreased considerably. To repeat, Figures 4 and 5 show how changes in proportional gain affect the response of the system. For many applications, this type of control is sufficient. However, better response can be obtained with a more complicated system.

Proportional Plus Derivative Control

Recall that the derivative term is a measure of how fast the servo motor is moving. The derivative component is added to the PID result in such a way as to slow the motor down. In Figure 4, we saw how the servo motor bobbed around the set point. Figure 6 shows how the servo motor responds with derivative control added. The resulting system is stable and has a good rise time.

A close comparison of Figures 4 and 6 reveals how derivative control functions:

- In both diagrams, the initial motor response is identical.
- The overall maximum speed of the motor is slower in Figure 6 (less slope).
- Since the maximum speed is less in Figure 6, the motor does not overshoot.

Just like the proportional control, there is a limit to how much derivative control may be added to the system, but too much derivative control will make the system unstable.

Proportional Plus Derivative Plus Integral Control

To understand integral control, we must first explore the limits of PID control. In Figure 7, we see how the servo motor responds under a load. The servo motor is unable to reach the set point; the blue and red lines do not merge.

From the previous discussion, we know this is a limitation of the proportional terms. We can rule out the derivative term, since it only functions to slow the motor down when it is moving fast. Recall from Part 1 that the proportional system only functions when there is an error.

The simple illustration in Figure 8 will help to explain why the proportional control is not able to eliminate the error. In Figure 8, we see that the motor is holding a weight stationary. Gravity is pulling against this weight. The motor must apply a torque which counteracts the effect of gravity. Without power, the motor would develop no torque and the weight would fall. Recall that the
proportional term is proportional to the system error. Therein lies the problem with proportional control. This one took a while for me to understand, but it makes sense when you think about it. The error cannot be eliminated. If the error was zero, the proportional drive would be zero, and the weight would fall. Therefore, in a set-up such as that in Figure 8, there will always be an error. The blue and red lines can never converge. In Figure 9, we see how the integral component can improve the steady state error of our servo motor system. Recall that the integral accumulates the error over a period of time. In Figure 9, we see that the servo motor has overshoot the set point, just like in Figure 7. Since the error is not zero, the integrator will start to accumulate the error. After a period of time, the integrator output is high enough to move the motor, as seen in Figure 8. The steady state error is, therefore, reduced.

To better understand the integral, let’s look at what happens when we increase the integral gain. As you can see from Figure 10, things can get ugly. There are two problems with this system: overshoot and oscillation. The overshoot is caused by the rapid accumulation of error. A large error exists for a period of time when the motor is commanded to move. This large error is accumulated by the integrator. This is called “integral wind-up.” If we were to look at the output of the integrator with an oscilloscope, we would see that the capacitor is fully charged, i.e., the integrator has saturated. This is not a good thing! Recall that the capacitor will not discharge until the error has changed signs. This means that the servo...
motor must overshoot to discharge the capacitor.

The oscillation seen in Figure 10 has an inherent problem with the integrator. The problem is with the very action of the integrator itself. Let me explain with an example:

1. Assume an error exists.
2. The integrator will accumulate this error over time. Therefore, output of the accumulator slowly rises.
3. The motor will move when the integrator output is sufficiently high. The required voltage level is determined by the motor inertia and the mechanical resistance.
4. Once in motion, the motor will continue moving.
5. In most cases, the motor will overshoot the set point and will start this process over again.

The overshoot is exacerbated by high integral gain. Unfortunately, the effect is also observed with low gains. The system may or may not settle at the set point. However, if the error is zero and the motor is not moving, the system will be in a state of equilibrium and all movement will stop. For the servo motor systems presented in this article, the settling process may take several seconds.

The operation of the integrator may be improved by the additional circuitry shown in Schematic 1. The analog switch we examined earlier helps to stabilize the integral. It does this by disabling the accumulation action if the motor drive is above a particular point.

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Figure 11 shows how the system’s performance is improved by adding the analog switch. The integral gain in this figure is the same as in Figure 10. The overshoot has been eliminated; unfortunately, the oscillation remains.

**Tuning Summarized**

Tuning a PID controller is like riding a bike. You have to keep your eye on system stability, rise time, and steady state error. I have the following rules of thumb to help you:

- Proportional gain determines how fast the system corrects a relatively large error. Increase the proportional gain for faster system response. If the term is too high, the system will overshoot and may oscillate around the set point.
- Derivative gain is adjusted after monitoring the system performance. Increase the derivative gain if the system has a large overshoot in response to step input. If the derivative gain is set too high, the system will again oscillate.
- Integral gain is adjusted to control the performance of the system when it is near the set point. Increasing integral gain will make the system quickly return to the set point. Decrease the integral gain if the system starts to oscillate.

My advice to you is to get out there and try to tune a PID system. We all learn best by doing. The servo motor system presented in this article is very responsive and easy to tune. The lessons learned are applicable to other systems. The worst that can happen is that you will strip a few gears! Also, read, read, read — there are many well-written texts to guide you in this process. As a starting point, I recommend that everyone get a copy of Professor Jacob’s *Industrial Control Electronics*.

Stay tuned; in Part 3, we will go high tech. We will take the lessons learned in the analog world and apply them to a digital PID controller. **NV**

**REFERENCE**

PLCs or programmable logic controllers are industrial grade stand-alone computers that typically do not have monitors, keyboards, or mice attached to them as they operate. A stroll through almost any industrial plant of about any size will usually reveal dozens and dozens of PLCs controlling industrial processes ranging from control of simple conveyor belts up to specialized industrial machinery designed to automate extremely complex manufacturing processes.

In the past, the PLCs themselves and the specialized software needed to communicate with and program them have been expensive and out of the reach of individuals outside of industry. Recently, Allen Bradley and Rockwell Software have been marketing the Micrologix 1000 bulletin 1761 series of PLCs that range in cost from $99.00 up to $189.00 for their most basic models (Photo 1). They are also offering their RSLogix 500 starter software for these basic models only as a free download from their website (www.ab.com).

There are other low cost PLCs and software available from other vendors, as well. This article, however, will only deal with the Allen Bradley Micrologix 1000 units. There are millions of PLCs being used in all aspects of manufacturing and in many other applications. Anyone working in the fields of electronics, computers, or programming can benefit from gaining a little knowledge about PLCs.

There is a lot of information that is needed to begin working with PLCs, so this will be the first article of two. This first installment will demonstrate how to begin programming in “ladder logic,” how to get a program into a PLC, and how to run and monitor the operation of a PLC program. The second article will present a more complicated ladder logic project — a roll-up door opener controller — and look at the way PLCs execute their programs. After reading these two articles, I am sure that you will come up with several PLC applications that you would like to implement.

Ladder logic programming is a graphical programming language adapted from ladder logic diagrams used by industrial electricians to hardwire relay logic circuitry. Using a graphical ladder logic program for programming PLCs has made the transition from reading ladder diagrams to writing software for PLCs easier for industrial electricians. For those who have already been involved in software programming, ladder logic programming will probably be quite a change, although most of the commands and features available in a typical programming language are available in ladder logic programming, as well.

To become proficient in PLC programming requires more information than can be put into a single article; this article is intended to be an introduction to get you up and going with simple examples. For further ladder logic programming examples and instruction, I recommend the text Technician’s Guide to Programmable Controllers, fourth edition, by Richard A. Cox. It’s published by Delmar and the ISBN is 0-7668-1427-0.

The first item to discuss will be which model PLC to purchase. Allen Bradley refers to their Micrologix 1000 family as “Bulletin 1761” devices. There are several models of Micrologix 1000 units available with several options to choose from in each model. The unit demonstrated in
this article will be the Allen Bradley catalog number "1761-L10BWA" model, which is their most basic 10-point PLC unit (see Photo 2).

There are three 10-point models available: the 1761-L10BWA, the 1761-L10BWB, and the 1761-L10BXB. All three models have six 24 VDC input terminals. This is what the first letter “B” in the part numbers refers to. The letter following the letter “B” is either a “W” for electromechanic relay outputs or an “X” for relays and 24 VDC FET (field effect transistor) outputs. All three units have four outputs. The third letter in the series is either an “A” for 120 VAC power or a “B” for 24 VDC to power the PLC itself. Other PLC models may have a number and a letter following those shown above; for example, “5A” would indicate that the unit has five analog I/O (Input/Output) pins.

Adding analog I/O to a PLC increases the cost substantially. To summarize, the basic Micrologix 1000 unit (catalog number 1761-L10BWA) demonstrated in this article has six 24 VDC input terminals, four electromechanic relay outputs, requiring eight screw terminals (two per relay), and 120 VAC to power the PLC itself. This unit has no analog inputs or outputs. The inputs and outputs are strictly discrete in nature or either ON or OFF. Therefore, this unit cannot be used to input analog signals, such as a varying voltage or current coming from a temperature sensor.

The first circuit that will be demonstrated on the PLC is a typical start/stop motor control circuit that is commonly found controlling industrial motors (Figure 1). In a typical hardwired start/stop circuit, the L1 line would be connected to the “hot” line of 120 VAC. The L2 line would be connected to the neutral or ground wire. The stop button is a normally-closed (NC) momentary push-button. The start button is a normally open (NO) momentary push-button. CR1 is the motor contactor winding.

The hold-in contacts parallel to the start button are auxiliary contacts on the motor contactor and will be closed when CR1 is energized. This contact allows the user to press and release the start button and not have to hold it in to keep the motor running. The actual motor itself and the connections to it are not usually shown on the ladder diagram. This circuit can be used to control the starting and stopping of any type of electrical motor.

If the start button is pressed and the stop button is not pressed, CR1 becomes energized and closes the hold-in contacts, as well as the actual motor contacts that will supply power to the motor itself. Since the hold-in contacts are closed and are parallel to the start button, releasing the start button will not de-energize CR1 and the motor will keep running. If the stop button is pressed, the power path to CR1 is broken, so the motor contactor releases and stops power flow to the motor, as well as to the hold-in contacts, and the motor stops. This would also occur if there was a power failure or if the start/stop wiring was damaged or if the NC stop push-button was not operating properly. The motor cannot start again — even if the power comes on after a power failure — until the start push-button is pressed.

Now, let’s connect this circuit up through the PLC and try it out. At this point in time, you may be asking the question, “Why use a complicated PLC to do what is already being done without a PLC?” This is a valid question. One answer to that question is that, once the circuit is operating through the PLC, many software options will become available and can be adjusted and experimented with quite easily through software changes without adding any further hardware items.

For example, if you wanted to make the operator hold the start button in for several seconds before the motor was actually energized — perhaps for safety reasons — the hardwired circuit would require more hardware like a delay-on timer. Using the PLC, we can simply add a delay-on timer in our software and easily change its settings at any time. To connect the push-buttons to the PLC, we will connect +24 VDC to one terminal of both the stop push-button and the start push-button.

The other terminals of each push-button can then be connected to any of the six inputs.
on the PLC — it doesn't matter which ones — but, for the sake of consistency, let's connect the stop push-button to the first input, input 0 (I0), and the start push-button to the second input, input 1 (I1). It will also be necessary to connect the negative side of the 24 VDC supply to the two DC COM or common terminals on the input side of the PLC. Supplying the positive 24 VDC to the input devices and connecting the negative to the DC COM terminals is referred to as sinking the inputs.

The opposite of sinking is sourcing of the inputs and can be done by connecting the positive 24 VDC to the DC COM terminals and the negative of the 24 VDC to the input devices. There are two DC COM terminals so that some of the inputs could be sourced and the others sunk, if desired. In this case, we'll keep it simple and sink all six inputs. When +24 VDC is applied to each terminal, it will become a “true” condition and its corresponding LED will light up. If you are going to connect the output of the PLC to a circuit at this time, be sure that it is compatible with the relay's voltage and current limitations of 24 VAC at 2.5A (Figure 2).

If your motor contactor requires a higher voltage and/or current than the PLC relays can handle, you'll need to connect an interposing relay between the PLC and the motor contactor that falls within the PLC’s relay ratings. When the PLC’s output becomes true, you will hear its relay click closed and see its corresponding LED light up. So, even if there is no load connected to the PLC, you can determine if it is working properly.

Now, it is time to enter the ladder logic information into RSLogix and get the compiled program into the PLC for testing. It is assumed at this point that RSLogix and RSLinx are already installed onto your PC. Open RSLogix and select the FILE | NEW pull-down menu. Scroll through the processor list until you find "Bul. 1761 Micrologix 1000." You can enter a processor name if you like at this time. If you give the processor a name — such as "STARTER" — then, whenever a PC is connected to the PLC, it will show the processor's name. This is important if your PLCs are networked together and you want to know which PLC is which by name or function.

After you select “OK” from the processor selection window, you should have a blank ladder diagram called "LAD2" with one rung numbered “0000” and the label “END” located on the right side of the rung. Now, you can insert new rungs by left-clicking on the rung number located on the left-hand side of the rung. Then right-click and, from the pull-down menu, select “insert rung.” You should now have two rungs visible — rung 0000 and rung 0001.

You can now place the ladder logic symbols onto rung 0000 by first selecting the rung, then left-clicking on the symbols from the user symbols tool bar located just above the ladder diagram window. Place an XIC (examine if closed) symbol — it looks like an NO contact — down for the stop push-button. Place another XIC symbol down for the start push-button and, finally, place an OTE (output enable) symbol — it looks like a pair of brackets — down
on the right side of the rung for the CR1 motor contactor coil. Your ladder diagram should look like the one in Figure 3.

If you are having trouble determining which symbol is which, simply place the cursor over each symbol shown in the user symbol tool bar and a pop-up label identifying it should appear. You may wonder why an XIC symbol looks like an NO contact, but is used for the NC stop push-button instead of an XIO (examine if open) symbol, which has a diagonal line through it like the NC contact symbol. The reason for this is that, when the stop button is not pressed, power will be applied to the I:0/0 screw terminal, making it true; when the stop button is depressed, power will not reach the I:0/0 screw terminal and the XIC test will be false. Therefore, the entire rung will be false. If an XIO symbol were used here instead, the operator would have to hold the stop and start buttons in simultaneously to get the output to be true or to come on.

We will add the hold-in contacts parallel to the start button at a later point in time. The question marks located above each symbol are there because we did not enter addresses for the symbols when we placed them on the rung. To enter their addresses, double left-click on the question marks and enter: I:0/0 for the stop push-button, I:0/1 for the start push-button, and O:0/0 for the OTE symbol on the right side of the rung. When you hit the enter key after entering each address, you will get a description and the symbol editor window. You can name each symbol, as shown in Figure 4.

Labeling the symbols is a nice feature because, once a symbol has been named, you can type in the symbol name rather than having to type in the address. Later, when the hold-in contacts parallel to the start push-button are added, we can type in “CR1” instead of O:0/0 and the software will assign the correct address to the label name automatically.

A few points about PLC addressing should be made at this time. Inputs are labeled with the letter “I” and outputs with the letter “O.” A colon then follows and then the number “0.” On other rack-mounted and expandable PLCs, other numbers may follow the colon, but this Micrologix 1000 PLC model is not expandable, so the first number following the colon will always be the number “0.” Next, there is a forward slash and, finally, the particular input or output terminal number. The possible input addresses for the six Micrologix 1000 10-point PLC inputs are: I:0/0, I:0/1, I:0/2, I:0/3, I:0/4, and I:0/5. The possible output addresses for the four outputs are: O:0/0, O:0/1, O:0/2, and O:0/3. Make sure to place a number “0” where necessary and not the letter “O” and vice versa.

Next, you can test your ladder diagram to see if RSLogix can understand and compile it properly. Do this by clicking on the verify project icon, which is a PC with a green check mark on it that is located above the user symbol tool bar. If there are no problems with your program, you will see the message, “verify has completed, no errors found” in the lower left corner of the screen. If errors are found, a window will appear at the bottom of the screen that will indicate which rungs have problems and which instructions on that rung have errors. Double-clicking on the error messages will cause the cursor to go to the symbol with that error.

Once the ladder diagram has been successfully verified, it is time to connect the PLC to the PC and download the program into the PLC. First, though, the communications software, RSLinx Lite, will need to be configured and enabled and the proper cable will need to be connected between the PC and the PLC.

Micrologix 1000 PLCs communicate through a special serial cable with the PC’s serial port. It is part number 1761-CBL-PM02, series B cable (Photo 3). The cable costs about $55.00.

Allen Bradley also supplies all of the necessary information needed to make your own cable. The cable uses an eight-pin male mini DIN connector on the PLC end and a DB-9 female connector on the PC end. Note, however,
that the eight-pin mini DIN connector is not the same exact connector as those found on a PC’s mouse or keyboard. Six wires are needed to make a cable and the DB-9 connector requires one loop-back wire to itself (Figure 5).

To open RSLinx Lite from Windows, select START | PROGRAMS | Rockwell Software | RSLinx | RSLinx. Then, select communications from the pull-down menu, select configure drivers, and click on the add new button. You can rename the RSLinx driver or leave it at its default name, AB_DF1-1. When the configure window opens, you can select auto configure if you are connected to the PLC or you can manually configure the settings, as shown in Figure 6.

Note that the communications set-up shown in Figure 6 is working through Comm Port 3. The laptop computer that this set-up was being demonstrated on uses com port 3 for the DB-9 male connector at the back of the PC. You can have all kinds of problems trying to configure and activate RSLinx if another device has taken control over the serial port first and vice versa. For example, I also use my laptop to synchronize my PDA through the serial port and, unless I go in and manually deactivate the serial port communications in my PDA software, RSLinx cannot open the serial port to reconfigure it. Also, RSLinx may come up when the computer boots up and take control of the serial port before other devices that need it can.

To prevent RSLogix from running all of the time, from Windows select: START | PROGRAMS | Rockwell software | RSLinx | Launch RSLinx Control Panel and then uncheck the “Always Run As Service” check box. You can also click on the stop button if you want RSLinx to stop running (Figure 7).

With RSLinx configured and running, you can communicate with the PLC and “Download” your program from the PC to the PLC or “Upload” what’s in the PLC to the PC. Let’s download the simple motor starter program by first verifying that the ladder diagram has no obvious errors. Then, go to the pull-down menu located in the upper-left corner that is now set at “Offline.” Change it to “Download.” You will then be prompted for a revision number; you can enter it or click “OK.” You are then prompted by a window which asks, “Are you sure you want to proceed with Download?” Select “Yes.” Next, a window will ask, “SLC is in remote RUN MODE, processor must be switched to remote PROG mode, continue?” Select “Yes.”
You will see an information window showing you the progress of the download. A window will then ask, “Change back to Run Mode?” Select “Yes.” Another window then asks, “Do you want to go Online?” Select “Yes.” You should now see the online/offline pull-down box displaying “REMOTE RUN.” The colorful ladder icon should also be spinning around, indicating that you are online with the PLC and your ladder diagram symbols should change to a green color as your inputs and outputs become “true.”

As you press your start and stop push-buttons, you should be able to turn the output relay on and off. You should also notice that you must hold the start button in to keep the output energized. We’ll learn how this can be fixed in the second article.

Well, that’s quite a bit of information to get started with, but it should have you talking with and programming your PLC with a simple motor start/stop circuit. In the next article, additional features will be added to the basic start/stop circuit and a slightly more advanced project will be introduced.
Small oversights can get you into trouble when you’re working with electronics. One factor to consider in every project — big or small — is ensuring that components do not overheat. Resistors, transistors, and other parts can get dangerously hot, even when you are not dealing with high voltage or lots of power. Basic thermal management is not difficult for most projects. Investing a little thought early on can keep you safe and save a great deal of reworking down the road.

The first step in thermal management consists of evaluating your circuit for potential trouble spots. Look for components that regulate the power supply — like voltage regulators, Zener diodes, or switching transistors. Power regulation circuits are common sources of heat because they pass the full current required by the rest of the system. Simple linear regulators dissipate a quantity of power equal to the product of supply current and input/output voltage differential.

A 5 volt circuit that draws just half an ampere from a 12 volt wall transformer will require a linear regulator to dissipate 0.5 A x 7 V = 3.5 watts; 3.5 watts dissipated in a confined space with inadequate precautions can quickly lead to a meltdown or worse. It is important to understand how much current your circuit draws from each voltage rail and what the power dissipation impact will be on the voltage regulators in your system.

Other parts of a circuit are candidates for heat trouble. Are you switching a load on and off? You may drive a light display. You may drive relays or solenoids to open doors or close valves. The switching components — which often include transistors, diodes, and resistors — can fall victim to heat-induced failure without proper design. High performance digital integrated circuits can run very hot. Running a state-of-the-art embedded controller at an internal clock frequency of 100 MHz or more can result in substantial heat dissipation. The high density of modern integrated circuits makes them ideal candidates for shedding lots of power in a small volume.

Thermal management — or cooling — seeks to spread power over a larger volume to reduce the maximum temperature in any one location. Cooling does not prevent your circuit from generating heat; cooling simply redistributes that thermal energy to prevent overheating — just like your car’s radiator disperses the engine’s heat.

**Thermal Analysis**

Once you have identified a potentially troublesome heat source, the next step is determining that component’s operating conditions. What is the maximum power it will dissipate? What is the maximum ambient air temperature that the system will operate in? You must consider the worst case conditions across all variables for a reliable solution. Finally, what is the component’s thermal resistance to ambient air? This is often a troublesome variable, but one that you have a degree of control over.

Thermal resistance defines the ease with which heat is conducted from a source to the ambient environment. A higher thermal resistance results in more heat build-up. Thermal resistance is often designated by the Greek letter theta — θ — and relates power and heat: DT = θP. θ is expressed in units of °C/W. The heat relationship tells us that a temperature rise results from a quantity of

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power multiplied by the thermal resistance through which the power is flowing. If a component is provided with a highly conductive thermal path to the ambient environment, its $\theta$ is low and, consequently, its temperature rise is low for a given power dissipation.

Finding $\theta$ for a given component is usually done by consulting the manufacturer’s data sheet. You can devise an experiment to obtain $\theta$ empirically, but such efforts are rarely necessary.

You can calculate a component’s maximum operating temperature when you know its maximum power dissipation, its thermal resistance to air, and the maximum ambient air temperature: $T_{MAX} = T_{AMBIENT} + \theta_{PMAX}$. If $T_{MAX}$ exceeds the manufacturer’s maximum rated operating temperature ...

"Houston, we have a problem!"

**Cooling a Hot Problem**

So what can you do when you run the numbers and $T_{MAX}$ is too high? It is always nice to have the luxury of redesigning a circuit for lower power dissipation. However, redesign is not always possible or practical. It would also be nice to lower $T_{AMBIENT}$ by only operating your system in Arctic temperatures. Again, this is not always practical. Generally speaking, you must find a way to reduce thermal resistance.

Two common methods of reducing thermal resistance are increasing airflow over the hot component and introducing a heatsink of some form into the system. When you place a fan near a hot component, the increased airflow results in more molecules of cooler ambient air passing over the heat source in a given time interval. There is more contact between hot and cold, resulting in a lower thermal resistance. You can observe this behavior at work in your computer, which has a fan in the AC power supply and probably has another fan positioned close to the CPU.

Metal is a far better heat conductor than air. Copper and aluminum are commonly used to fashion efficient heatsinks. Aluminum is the preferred material because it is less expensive than copper. You will find copper heatsinks in leading edge circuits where the heat problem is so severe that copper’s higher cost is justified.

The basic purpose of a heatsink is to efficiently conduct heat away from a dense source and spread that heat over a much larger area, where it can be properly carried away by the ambient air. A fan’s presence increases the effect of a heatsink because the moving air more rapidly conducts heat carried by the heatsink.

The overall thermal resistance from the hot component to the air is what matters in our analysis. This total resistance is the sum of all the heat conductors and their interfaces.
CPU in your computer has a certain thermal resistance between the silicon and the CPU package. There is a thermal resistance between the package and the heatsink. There is also a thermal resistance between the heatsink and the moving air. Summing all of these resistances gives the total $\theta$.

Comprehensive thermal analysis is worth further investigation. There are numerous sources of data on the web and in print.

**A Hot Voltage Regulator**

Returning to our original example, suppose we are dealing with a 5 V linear regulator — such as the LM7805 — which is called upon to dissipate 3.5 W. The LM7805 is commonly available in a TO-220 package, which has good thermal properties for its small size: a thermal resistance to air of 65 °C/W. Let's do the math, neglecting ambient air for now: $DT = \theta P = 65 \degree C/W \times 3.5 W = 227.5 \degree C$. Ouch! We could briefly boil water before melting the solder and perhaps starting a fire. Something must be done.

Fortunately, the TO-220 is designed to accept a heatsink and many standard off-the-shelf heatsinks are readily available. The TO-220’s thermal resistance to its package is just 2.5 °C/W. You can observe how most of the resistance is due to poor heat transfer in air. Off-the-shelf heatsinks for TO-220 packages can be found with thermal resistances under 3 °C/W in still air. That yields an overall $\theta$ of approximately 2.5 °C/W + 3 °C/W = 5.5 °C/W. The temperature rise is looking much better now: $DT = \theta P = 5.5 \degree C/W \times 3.5 W = 19.25 \degree C$. If the regulator’s maximum operating temperature is 80 °C, the device can now operate up to 80 °C – 19.25 °C = 60.75 °C. This exceeds the vast majority of requirements.

**Stay Cool**

You should always examine your circuit before building it to ensure that it will operate safely. This includes proper thermal management. The worst consequences of inadequate cooling include damage, fire, and serious injury. Even if a circuit does not cause immediate damage or injury, heat is a silent killer of electronics. Heat exposure over time shortens the life of your components. A cooler circuit will last longer than its comparable, hotter counterpart and improve safety.

**About the Author**

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Digital Signal Processing (DSP) is an art that has been applied to most every aspect of our everyday electronic existence. Your stereo’s CD player probably employs DSP technology and, if you own a fancy wireless home telephone, it will also most likely call upon the services of DSP.

DSP is what you make it. You may only want to average some incoming signal levels over time or you may want to analyze the frequency spectrum of a signal. DSP techniques can be simple or complex. So, rather than attempt to bang out a particular DSP project that may or may not be something you wish to read about, I’ll describe the basic elements of a DSP project and let you fill in the middle of the pudding with your favorite mix of flavors.

As you know, I began this DSP discussion by describing a dsPICDEM demo board from Microchip and I’ll continue to use that piece of hardware in this offering. The dsPICDEM 28-Pin Demo Board is an unassuming little board that contains a 28-pin variant of the Microchip dsPIC family of devices. Despite the low pin count, the dsPIC30F2010 contains everything you will need to perform some DSP magic of your own. Grab a copy of the dsPIC30F2010 data sheet and follow along as we take a detailed look at one of the most important DSP subsystems that are embedded within the dsPIC30F2010 package.

The dsPIC30F2010 Analog-to-Digital Converter

To be able to perform DSP operations, you must have an incoming signal to process. That signal, if it is analog in nature, is normally acquired by an analog-to-digital (A/D) converter. Remember, the object is to get as much of the original signal’s information into the DSP engine as possible. To do this, the A/D converter must be fast and accurate relative to the incoming signal.

The dsPIC30F2010’s A/D converter resolves to 10 bits, which equates to 1,024 steps, including the zero step. That means we can use the dsPIC30F2010’s A/D converter to convert an incoming voltage to a 10-bit digital number. Since the dsPIC30F2010’s A/D converter is rated at a maximum of 500 ksps (kilosamples per second), we can do our voltage level collecting very quickly, depending on how fast we run the dsPIC30F2010 CPU.

Just in case more than one voltage source needs to be sampled, the dsPIC30F2010’s A/D converter multiplexes six input channels into four sample and hold amplifiers. The sample and hold amplifiers do just what their name implies; they sample the incoming input signal and hold that value for use by the A/D converter circuitry behind them.

Think of the sample and hold amplifiers as analog output channels (CHO, CH1, CH2, CH3) with multiplexed inputs (AN0, AN1, AN2, AN3, AN4, AN5). One, two, or four of the dsPIC30F2010’s sample and hold amplifiers can be enabled to acquire the incoming data. This allows differing sets of analog inputs to be selected and scanned. For instance, input AN0 can be switched into CH0 or CH1. However, CH1 can only take input from AN0 and AN3, while CH0 is capable of accepting analog input from all six analog input pins. Regardless of the origin of the analog input, the digital A/D converter results are stored in locations 0x00 through 0x0F in the 16-word result buffer — ADCBUF — which is addressed ADCBUF0 through ADCBUFF.

Configure the Analog I/O

Let’s explore the dsPIC30F2010’s A/D converter by configuring it and reading some input voltages. The first step in the dsPIC30F2010 A/D converter configuration process is to identify and set up the analog input pins by setting up the ADPCFG register. The dsPIC30F2010’s ADPCFG register is 16-bits wide, but only uses the lower six bits, as six input pins are all we have for analog inputs. Writing a “0” (zero) to a bit position in the ADPCFG register reverts the corresponding input pin to analog input mode. A “1” written to a bit position in the ADPCFG register forces the I/O pin to the digital mode.

Since we’re only interested in analog input at this juncture, let’s fill our ADPCFG register’s lower six bits with zeroes and enable all of the analog inputs on PORTB. We will also need to set the TRISB register to 0x3F, which directs RB0 through RB5 to turn off their port I/O drivers and work as input pins. Failing to correctly TRIS the PORTB analog inputs and input pins forces the A/D converter to read the level on the pin’s output driver instead of the incoming analog voltage.
Establish the A/D Converter Voltage Reference

Now that we’ve designated the analog inputs, the next step is to establish a voltage reference for the A/D converter. The dsPIC30F2010 has provisions for both positive and negative A/D converter reference inputs. Let’s keep our implementation simple and use the PIC’s voltage rails as the upper and lower limits of our measurements.

The dsPIC30F2010’s AVDD and AVSS pins are connected to a filtered +5 VDC voltage source, which is native to the dsPICDEM 28 Pin Demo Board. This +5 VDC powering of the AVDD and AVSS pins places the dsPIC30F2010’s A/D converter measurement limits equal to the voltage rails (0 and +5 VDC) of the dsPIC30F2010. To associate our physical voltage limits to the dsPIC30F2010 A/D converter circuitry, we must also zero the VCFG (Voltage Reference Configuration) bits, which are the three most significant bits of the ADCON2 register.

Now, the physical voltage reference matches the voltage reference configuration register definition. By setting the rest of the ADCON2 configuration register bits to zero, we choose to only convert inputs muxed to CH0 and to not scan a series of analog input pins. We haven’t talked about analog input scanning. In a nutshell, the dsPIC30F2010 A/D converter has the capability of scanning a set of analog input pins automatically. We’ll get a simple conversion process going first and then look at how to make the A/D converter scan.

Clocking the A/D Converter

Although we know that the dsPIC30F2010 A/D converter zooms, it still has its limits. It takes time to sample and then convert the sample. This sample and conversion timing is controlled by the analog module clock and is measured in a number of clock periods designated as TAD.

A TAD is defined as one analog module conversion clock period. A single dsPIC30F2010 A/D conversion requires a minimum of 12 TAD periods. We can choose to get our analog clock periods from an internal RC oscillator from the instruction clock. The minimum TAD time required for a successful A/D conversion is 154 nS. We control TAD timing using the lower six bits (ADCS) of the ADCON3 register. Here’s how we determine the correct ADCS value:

\[
\text{ADCS} = 2 \times \left( \frac{\text{TAD}}{\text{TCY}} \right) - 1
\]

Where:
- \( \text{TCY} = 1 / \text{instruction clock} = 1 / (4 \times 7.3728 \text{ MHz}) = 34 \text{ nS} \)
- \( \text{TAD} = 154 \text{ nS} \)

Instruction clock is in XT 4x PLL mode.

We can’t designate a fractional ADCS value. So, we can round our ADCS value to 8. Checking our work

<table>
<thead>
<tr>
<th>Listing 1</th>
</tr>
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```c
#include <string.h>
#include <stdio.h>
#include "delay.h"
__CONFIG(FOSC,POSC & XTPLL4 & CLKSWDIS & FSCMDIS);
__CONFIG(FWDT,WDTDIS);
__CONFIG(FBORPOR,PWRT16 & MCLREN & BORDIS);
__CONFIG(FGS,GCPU & GWRU);
__CONFIG(FCOMM,PGEMU);
#define BAUD1 57600
#define OSC1 7372800
#define DIVIDER1 (((OSC1/BAUD1) /16) - 1)
void putchar( char c);
void putchar( char c)
{
    while(!U1_TRMT); //TRMT is set when TSR is empty
    //continue;
    U1TXREG = c; //load the register
}
void main(void)
{
    char x;
    U1_ALTIO = 1;
    U1BRG = DIVIDER1;
    U1_UARTEN = 1;
    U1_UTXEN = 1;
    // echo code for demonstrating UART operation
    // use HyperTerminal to see the echoed characters
    // as you type them.
    // while(1){
    //    while(!U1_URXDA);
    //    while(!U1_TRMT);
    //    U1TXREG =U1RXREG;
    //    U1RXREG =UIRXREG;
    // }
    ADPCFG = 0x0000; //all PORTB I/O = Analog input
    TRISB = 0x3F; //all PORTB I/O = input
    ADCON2 = 0x0000; //no scan, GDO only
    ADCON3 = 0x0009; //170 nS Tad with system clock
    ADCHS = 0x0000; //sample AN0
    ADON = 1; //turn on the ADC
    while(1){
        //ADIF = 0; //clear the ADC interrupt flag
        AGSM = 0; //set up for manual conversion trigger
        SAMP = 1; //begin sampling
        x = 10; //delay for sampling to be performed
        while(!x); //wait for ADC conversion to complete
        printf("\r Input Value = %4X",ADCBUF0);
    }
}
```

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using the rounded ADCS value:

\[ T_{AD} = \left( \frac{TCY}{2} \right) \times (ADCS + 1) = 153 \text{ nS} \]

Where: \( ADCS = 8.0 \)

Doing the “check our work” math for \( T_{AD} \) — again using the entire original computed ADCS value \( (8.0832896) \) — does provide the expected answer of 154 nS. However, since we can’t include the fractional value of ADCS, we can meet our minimal \( T_{AD} \) figure by simply upping the computed ADCS value to 9, which yields a \( T_{AD} \) of 170 nS.

**Define the Active Analog Input Pins**

Up to this point, we have selected our analog input pins, specified the A/D converter reference, and identified and configured the A/D converter clock source. The next step is to choose which analog input or inputs to sample. This is accomplished by setting up the ADCHS register. The upper byte of the ADCHS register is dedicated to what is termed MUX B, while the lower byte of the ADCHS register represents MUX A.

Put simply, a MUX is a defined set of pins you desire to sample. The movement between the pins set in MUX A versus the pins selected in MUX B is determined by the ALTS bit, which is bit 0 of ADCON2. Since the least significant bit of ADCON2 is cleared in our application, our code will operate on analog input pins defined in the MUX A area of the ADCHS register. The four least significant bits of the ADCHS register determine which analog input pin is selected for sampling. Thus, a value of 0x0000 for ADCHS will set up MUX A with analog input AN0 on CH0 as our sample input. A value of 0x0001 selects AN1 on CH0 and so forth. Believe it or not, the configuration is finished and we’re ready to power up the dsPIC30F2010’s A/D converter and read some voltages.

**Power Up and Test the Code**

Listing 1 is a culmination of what we have discussed thus far. For those of you who may have missed the first installment of DSP theory in the December 2004 issue of *Nuts & Volts*, I’ll quickly explain the UART code you...
see at the beginning of Listing 1.

If you continue to follow "Design Cycle," you’ll notice that I always like to establish a baseline serial interface. Once you get the serial port of that microcontroller working, other things just seem to fall into place a little easier. Recall that I modified my dsPICDEM 28-Pin Demo Board to allow me to use the alternate dsPIC30F2010 serial port so I could eliminate the need to move jumpers to enter and exit debug/program mode with the MPLAB ICD2.

The U1_ALTIO = 1 statement tells the dsPIC30F2010 to use the alternate USART signal pins. The dsPIC30F2010's UART is enabled by setting the most significant bit of the U1MODE register (U1_UARTEN = 1). The dsPIC30F2010's UART baud rate can then be calculated with the following formula:

Baud Rate = Fcy / (16 * (BRG+1))

Where: Fcy = Instruction Clock Rate
BRG = Value to load into U1BRG for baud rate clock generation

The DIVIDER1 macro statement in Listing 1 solves for the correct BRG value. The baud rate generator value generated by the DIVIDER1 macro is then loaded into the U1BRG register using the statement U1BRG = DIVIDER1. Once the baud rate generator is loaded and the UART is enabled, the UART transmitter is switched on by setting the UTXEN bit in the U1STA register (U1_UTXEN = 1).

The commented-out code between the while(1) braces in Listing 1 is a simple serial echo mechanism. The dsPIC30F2010 UART has its own four-byte receive and transmit buffer. When a character enters the receive buffer, the URXDA bit is set. If there is no transmission in progress, the TRMT bit will be clear. The little echo code snippet waits for a character to enter the receive buffer and, when all is clear on the transmit side, it moves the incoming character from the receive buffer into the transmit buffer for transmission. If you wish to run the echo code, simply remove the comment slashes.

Okay, back to the dsPIC30F2010's A/D converter. As you can see in Listing 1, all of the A/D converter set-up is performed just before turning on the A/D converter module. Once a conversion is complete, the A/D conversion interrupt flag, ADIF, is set. We’ll poll the ADIF flag to determine when the current A/D conversion has completed. We could also poll the A/D conversion DONE bit in a similar manner to the ADIF flag bit with the same results. The ASAM bit is cleared to indicate to the A/D converter module that the setting of the SAMP bit (bit 1 of ADCON1) will be the signal to begin sampling the selected analog input pin.

After setting the SAMP bit, some time must be given to the sampling
process. Once the input signal is sampled, clearing of the SAMP bit starts the A/D conversion process. When the ADIF flag signals the end of the conversion, read the digital result from the ADCBUF0 register and display it as a hex value via the dsPICDEM 28-Pin Demo Board’s serial port and a HyperTerminal 56K asynchronous terminal session. This sample/hold/convert/display process runs until you reset or power off the dsPIC30F2010.

**Scanning Multiple Analog Inputs**

I briefly mentioned scanning earlier and promised to show you how it is done. Take a look at Listing 2. It’s basically the same code we used to harvest a voltage from AN0. The only configuration changes that I had to make involve ADCON2 and the addition of ADCSSL. In the upper byte of ADCON2, I switched on the CSCNA bit (0x04XX), which turns on the scan input function. The lower byte of ADCON2 sets a bit pattern inside the SMPI (Sample/Convert Sequences Per Interrupt) selection bits (0xXX04). The SMPI bit pattern instructs the A/D converter subsystem to set the ADIF interrupt flag after two analog inputs have been sampled and converted. By placing a “1” in the 0 and 1 bit positions of the ADCSSL register, I’ve indicated that I wish to scan only AN0 and AN1. The only other change to the configuration is the setting of the ASAM bit, which is required when scanning.

The rest of the code is really easy to follow. First, I clear the ADIF flag and kick off the sample process for the first analog input pin to be scanned, which is AN0. I wait for a period of time and trigger the A/D conversion of the sampled AN0 input. The result of the conversion is stored in ADCBUF0. The same procedure that was used to collect the voltage at pin AN0 is repeated for analog input AN1 with the AN1 conversion result being stored in ADCBUF1. The ADIF flag is set following the second sample and conversion indicating that the scanning is complete. I then can retrieve the results of the two A/D conversions and display them via the dsPIC30F2010 serial port.

**End of Conversion**

Getting an accurate representation of the analog data you wish to process using DSP concepts is essential. Now that you have a grasp of the basic operations associated with the dsPIC30F2010’s A/D converter, you can take the first step in creating your own DSP application. If you study the dsPIC30F2010 data sheet and the companion dsPIC30F Family Reference Manual carefully, you’ll find a multitude of ways to deploy the dsPIC30F2010’s powerful A/D converter.
In the December issue, I described how I was getting back into ham radio after a long hiatus by building some kits. The kits I chose are made by Ramsey Electronics of Victor, NY. They are very low in cost and simple, even for a beginner. I built the HR30 receiver kit first to get familiar with the 30 meter band before launching back into the hobby. The receiver is a simple, direct conversion type and works very well with its varactor tuning.

Refer back to the December issue for all of the details. In this article, I will describe my experience with the QRP30 transmitter and the QAMP30 optional power amplifier.

The Transmitter

The QRP 30 is designed for the 30 meter ham band that covers 10.1 to 10.15 MHz. That is only 50 kHz wide, but it's enough for ham CW work. The transmitter is a QRP (low power) design that has a maximum output of about 1 watt. It doesn't sound like much, but it truly is amazing what you can do with low power if you have a good antenna and reasonably good conditions, as well as some patience.

The basic circuit is shown in Figure 1. Q1 is just a basic crystal oscillator of the Colpitts type. It has provisions for two crystals. The one I got was for 10.108 MHz, just inside the low end of the band. A push-button switch selects between the two crystals. I did not invest in another crystal, as I did okay with the one I had.

Besides, the circuit provides a pair of varactor diodes that can be used to “pull” the crystal frequency over a narrow range. Why don’t you take a look at the circuit in Figure 1 with diodes D3 and D4. A 10K pot, R1, varies the DC bias to change the varactor capacitance that, in turn, gives about a 5 kHz variable frequency range around the crystal frequency.

The oscillator output is fed to an intermediate buffer driver amplifier, Q2. This amplifier isolates the crystal oscillator from the final amplifier to prevent frequency variations. It provides sufficient output to drive the final amplifier, Q3. The final stage is a class C amplifier. Its collector output drives a Butterworth low pass filter made up of C17, L6, and C18. This filter matches the transistor output impedance to the 50 ohm output impedance for the antenna. It also serves to greatly reduce any harmonics generated in the class C amplifier. Using a 12 volt power supply, you should get about 1/2 watt output. The output will go to about 1 watt with a 15 volt supply.

Looking at Figure 1, note the circuit at the top using transistor Q4. This PNP is used as a switch to turn the DC supply off and on in accordance with the state of the external telegraph key connected to jack, J3.

With the key up, there is no bias on Q4, so it is off and the transmitter does not get any power. When you press the key down, Q4 gets forward bias and conducts heavily, applying the full 12 volt supply to the crystal oscillator and the bias resistor, R8, for...
Open Communication

the driver stage. The oscillator signal is then amplified and appears at the antenna jack, J1.

As the transmitter is keyed, it also automatically operates the transmit/receive (T/R) circuit at the transmitter output. It consists of diodes D1 and D2 and their related components. When the transmitter is not keyed, D2 is biased on by the voltage through R13. The voltage on the cathode of D2 keeps D1 cut off.

At this time, the signal from the antenna passes through the low pass filter, C10, D2, and C19 to the receiver. When the key is pressed down, 12 volts are applied to D1 through L4, turning it on. The voltage at the cathode of D1 reverse biases D2, so none of the transmitter signal gets through to the receiver. The class C amplifier output passes through D1 to the low pass filter and the antenna.

Testing the Transmitter

You will need a power supply, a key, and some kind of dummy load. If you have a receiver that would help, too, as you will be able to actually hear the signal, which is always a good test.

As for a power supply, you need at least 12 volts DC at 500 mA, minimum, for a 1/2 watt output. A supply of 15 volts will get you to the 1 watt output level. Any well filtered and regulated supply can be used.

If you do not have a supply, you can actually use eight D cells in series to give you 12 volts. Using 10 D cells will give you the 15 volts needed for maximum output. They certainly have the capacity to supply the current for many hours of operation.

You can also use one of those wall plug transformer supplies that are so common on battery chargers. Be sure to get one with 12 or 15 volts and at least a 500 mA rating or, better still, 1 amperes. My experience is that these are not too well filtered and certainly are not regulated, but they are convenient. You can also build yourself a supply from scratch or buy one of the many kits available.

While you are at it, get a 2.5 mm power plug that comes with the wall transformer supplies, as that is what is used for the DC input on the transmitter kit. I had to go buy one to connect my supply — an old Heathkit supply I used to use on a two-meter transceiver sometime back.

As for a key, I had an old standard telegraph key that I have used for decades. It is still in great shape and, after I cleaned it up, it looks like new. They don't build them like they used to. I do have an old Heathkit keyer somewhere and I will probably use that — once I find it and get some practice with the code again.

If you read my receiver article in the December 2004 issue, you know how I feel about the coax connectors used on these kits. All of the inputs and outputs use RCA phono jacks.

Continuing my rant here, I hate these things. If you didn't know, these things were invented back in the 1930s by RCA for connecting record players to radios and/or amplifiers. Yes, they were made for audio, not RF. However, they do work on RF and video. Most audio and video connections in stereos and TV sets are still using RCA connectors.

Anyway, for RF, the regular UHF SO-239 jack and PL-259 plug are better, although more expensive. They are also a bit easier to work with than the RCA connectors. They give a better match to the coax and have lower loss.

Yet, they do take up more space and cost more. On the other hand, they are a better fit when using test equipment and cables in ham work.

In any case, I spent more time fussing with the cables and connectors than I did in building all the rest of the kit. Bummer. Mike Leo at Ramsey said they were aware of this deficiency and hoped to correct it in the future.

Believe me, Mike, most of us would pay a few bucks extra just for this. I took the easy way out by buying coax adapters from All Electronics to convert PL-259s to the phono jacks. They were a bit expensive, but well worth the cost. If you have ever spent time putting connectors on coax, you know it is.
Building the Power Amplifier

If you are just not satisfied with 1 watt of power or less, you can get Ramsey’s QAMP30 — a 10-20 watt power amplifier that can be driven by the QRP30 transmitter. The circuit is shown in Figure 2. This transmitter uses a pair of enhancement mode MOSFETs in a push-pull circuit. It is a broadband (untuned) design that can be used over a wide frequency range.

In case you haven’t noticed, MOSFETs are taking over the world. Over 90% of all semiconductors made today are MOSFETs, integrated or discrete. They are easier to work with than bipolars and have higher input impedances. You can buy power RF MOSFETs that are good for powers of up to 300 watts or so. These devices have essentially replaced bipolars in most RF (and audio) power amp applications these days.

The 1 watt signal from the QRP30 transmitter comes in through J2 and passes through relay K1 and is applied to the primary of transformer, T2. This transformer matches the 50 transmitter output impedance of the QRP30 to the input impedances of the MOSFETs while also providing 180 degree out-of-phase signals to the MOSFET gates. The power MOSFETs operate in push-pull, meaning that on the positive half cycle of the input, Q1 conducts while Q2 is cut off. On the negative half cycle of the input, Q2 conducts while Q1 is cut off. The transistors amplify only half of the signal, which is then reassembled in the output transformer, T1. T1 matches the output impedance of the MOSFETs to 50 ohms for maximum power output. The output goes to a five-pole low pass filter made up of L1, L2, L3, and C4 through C7 and then to J1. The filter effectively reduces any harmonic output.

This amplifier is pretty linear, therefore it has minimum harmonic distortion to begin with. The
MOSFETs are actually biased on a slight amount, making them operate in class AB. This gets rid of any crossover distortion common in push-pull transistor amplifiers. The bias comes from the 6.2 volt zener diode, D1. It operates from the 12 volt supply. Its output goes to a 5K pot, R4, and through R5 to the center tap on the secondary of T2, and then to the gates of Q1 and Q2. The bias is adjusted to 5 volts during the initial tests.

This amplifier uses an RF operated relay for transmit/receive switching. Looking at Figure 2, you can see the RF coming in from J2. It is applied to a voltage doubling rectifier made up of D2 and D3. The DC created by this circuit biases the Darlington pair Q3 and Q4 on. This does two things.

First, it energizes the coil to relay K1. K1’s contacts connect the RF input to T2 and J1 to the output filter.

Second, it turns on Q5, a switch that energizes the bias circuit turning on the MOSFETs. And, voila, the amplified output appears at J1. J1 connects to the antenna.

As for the construction, it is pretty easy and not unlike building the QRP30 transmitter. The only tricky part was winding the coils and transformers. The kit comes with three toroid cores and the ferrite cores for T1, T2, and the wire.

None of this is difficult, but it is a bit time consuming — but, hey, remember, this is a kit and it does take time. Consider that part of the fun. As I suggested in my December article, take your time to avoid mistakes that can make your life hell when you go to power up the circuit.

Incidentally, Ramsey does sell some nice enclosures for these kits. I did not use them, but — if you want to make things look neater — these nice boxes come with knobs and the end result is a professional-looking product.

**Testing the Power Amplifier**

You will need a honking big power supply to power this thing. Get a supply that will give you 12 to 15 volts up to 3 amps. I didn’t fool around with trying to build anything this big, so I just bought a surplus supply.

Also, don’t forget the dummy load. Again, Ramsey suggests a light bulb, which does a great job. A #93 auto bulb is good for about 10 watts of output. Use a #1156 auto bulb for up to 25 watts output. You can also build yourself a dummy load with resistors, as suggested earlier. I used 10 510-ohm, 2 watt resistors in parallel to give me 51 ohms at 20 watts. Be sure NOT to use wire-wound resistors that have too much inductance for RF work. Use regular composition or metal film resistors.

I connected the QRP30 output to the QAMP30 input with a short coax cable with RCA phone plugs on it. This is a 75 ohm cable used for video, but — since it is short — there were not any SWR problems and I didn’t have to fuss with installing connectors on a 50 coax cable. With 1 watt of drive power from the QRP30 and 12 volts, there is an amplifier current of about 1.5 amps. This is good for about 10 watts output.

I used the bulb dummy load, which worked fine. My MFJ-816 RF power meter read about 8 watts. You can get more output if you go to a 15 volt supply. With 1 watt input power, the output goes to about 12 watts. You need more RF input drive power to get to the 20-25 watt output potential of this amplifier.

Nevertheless, a boost for 1 watt from the QRP30 to 10 watts produces excellent results. It makes it much easier to make contacts so is worth the price.

Checking the output power and SWR with my MFJ-816 power meter, I read an SWR of about 1.6 with my 30 meter dipole. Not bad. Anything less than an SWR of 2:1 is good.

So, now I am back on the air. I forgot how entertaining it could be. My CW speed is picking up. Now I am aching to get on some of the other bands to see what is going on. Eventually, I may break down and buy a big, multiband transceiver. In any case, these Ramsey kits have been fun to build. They have also provided a quick, low cost way to get back to ham radio. **NV**
Q

uality and quality control are important to the success of any product. Designing and producing a quality product is not accidental. In this column, we will examine those factors that are necessary for creating and manufacturing a quality product. We will also briefly touch on the ISO 9000 quality standards.

Definition

Quality, or its lack, means different things to different people. This is not surprising. People are not all the same. For example, parents think that their children’s music is toneless noise. Children think Mozart “eats dead rats.” We will strictly define quality as “something that meets well-defined, objective standards or specifications.”

Of course, these standards and specifications may be easy or hard to achieve. Worse, similar products may have vastly different specifications. This means that a product that performs poorly may actually have better quality. Here’s how.

Suppose there are two manufacturers that make stereo amplifiers. One manufacturer specifies 1% distortion. The other specifies 0.001% distortion. It’s clear that the manufacturer of the 1% distortion amplifier has a much easier task in terms of design and production. It is also clear that it is a “lower quality” amplifier in terms of performance. He should have very little trouble in making a product that consistently meets the 1% distortion specification. Conversely, it’s harder to design and produce an amplifier with 0.001% distortion. This manufacturer is very likely to see many more instances where the product fails to meet that standard of performance. By this measure, it is a “lower quality” amplifier.

The point of this is to show that “quality” has a different meaning from the common use of the word. My personal preference is to use the term “reliability” instead of quality. It seems to be a better description. However, I doubt that all the quality control departments are going to change their names soon. Therefore, the definition of quality remains, “a product that meets objective standards or specifications.”

Attitude

Arguably, the most important aspect in achieving quality is attitude.

If you have great pride in your work, you will automatically strive for a quality product. You will want to do the best that you can. You will see your product as a reflection of yourself — and no one wants to look bad.

On the other hand, if a company president announces a wage freeze while accepting a huge bonus for increased profits, you may not care much about quality. You may just go through the motions with little concern.
about the product. This is just human nature. What we see is that businesses that foster good company spirit, respect for employees, and teamwork will generally have an easier time making quality products. We also see that the quest for quality must be initiated and supported by the highest levels in the company. This also means that management actions that would undercut these factors must be avoided (even if this means a smaller bonus for the president). Fundamentally, a happy employee does better quality work than an unhappy one.

**Education**

Of course, wanting to do something and actually doing it are two different things. Education, training, and experience are vital in any successful endeavor. Quality is no exception. Designers must feel comfortable and confident in making ideas into reality. Production must know the limitations of their equipment. Technicians must understand the important aspects of the product. These people must also communicate with each other in order to foresee and avoid problems in any particular area.

Because of the rapid changes in engineering, this education must be ongoing. Learning must never stop. Like Alice in Wonderland, you have to keep running as fast as you can just to stay in the same place and be competitive. And, in order for this learning to be effective, it must be communicated to all affected groups in the company. New surface-mount equipment in production will be wasted if the designers aren’t aware it exists.

A significant part of education is documentation. Documentation teaches. No one will deny the vast impact that writing had in the history of the human race. Yet, these same people may think that documentation is for someone else, not them. After all, they designed the system, so they know all about it. Thus, it’s not important. Actually, they’re almost exactly correct.

Documentation really is for someone else. It’s for someone else who doesn’t know as much as the designer, but — for that very reason — it’s critical information for the newcomer. Designers seem to overlook this point. I’ve heard many engineers complain about the lack of documentation when assigned to a new project. Yet, these are often the same people who dismiss documentation as boring and unnecessary.

**Product Quality**

I have one product that I marvel at every time I use it. It’s my Ford 8N tractor. It was built in the early 1950s, so it’s about 50 years old. Since I’ve owned it (about 20 years), it’s been kept outside and fully exposed to the weather. Not only does the tractor still run, it runs well. A few years ago, I bought a new (yes, new!) wiring harness for it for about $25.00. Think about that. They are still making wiring harnesses for a 50-year-old farm tractor!

I suppose everyone has a similar story. I also suppose everyone has horror stories about products that are simply abysmal.

**Design for Quality**

How do you design a quality product? Truthfully, it’s not that hard to do. You need a full set of reasonable specifications. (Fantasy, contradictory, and mutually exclusive specifications are not reasonable.) There must be a reasonable amount of time for research and testing. Appropriate tools must be available. The design must match the manufacturing capabilities. If this sounds like common sense, it is. Unfortunately, common sense isn’t all that common. Every engineer can provide loads of examples where designers were given vague specifications that were constantly changing, a time frame that was absurd, or tools that were simply not adequate. Production can also give examples of designs that simply can’t be built with the equipment on hand. (Or perhaps with any equipment in existence.)

For the design engineer: Keep everything as simple as possible. The fewer the parts, the fewer the things that can fail. Don’t push components to their limits. Sometimes, you can get increased voltage or current ratings on components with little or no increased expense. (This requires communication with the purchasing department.) Use large traces and spaces on PCBs (printed circuit boards) whenever practical. Don’t use a common and
inexpensive PCB auto-router.

If it’s a simple board, it should be easy to lay out manually. If it’s a complex board, the auto-router can really mess things up. (A high current switching line routed next to a feedback line will cause problems every time.) Understand the manufacturing process and work with it. Design your product around your personal strengths, as well as your production department’s strengths.

For the production department: Engineering does not deliberately make things difficult for you. The changes in the field of engineering are usually much faster and larger than those in production. This means that production has to learn to adapt quickly to new procedures and techniques. Try to anticipate changes by keeping up-to-date on new developments. This requires effort. Subscribing to trade journals (and actually reading them) is a good thing to do.

Teach the engineering department about what is possible and what isn’t. Often times, they simply don’t know. Every new engineer should have a tour of the production facilities. When new equipment is obtained, engineering should be notified about its capabilities. Let the engineering department be aware of any special strengths that you have. Perhaps they can design the product around that. As you can see, communication is important and cannot be ignored.

For the engineering manager: Understand that quality is a team effort. Use the expertise of your people and respect their judgments. If you ask your engineer how long it will take to develop a new product, believe him. If he says 10 weeks and you reply, “I’ve already told our client (or president) we can have it in four weeks,” you are simply being stupid. That’s strong language, but it’s the truth (and no one else will tell you).

The only truly valuable assets of any company are its people. Not using your assets to their fullest is not a smart thing to do. The result will be quite predictable. Either you will have a poor product that the customer will not be happy with or you will have a product that will be late. In that situation, the customer will also be unhappy. In most instances, both will happen and your reputation will be that of someone who can’t deliver.

As the manager, you must lead by example, not by fiat. Quality is not something that can be added at the end of a product’s design. It is inherent to the people who design and manufacture it (stress people). If there is a need for a four-week design cycle, discuss it with engineering and production. Find out what is realistic. Then discuss it with the client/president. It is very rare that a reasonable compromise cannot be reached. This is called negotiation and it is part of the manager’s job. The result is a quality product, on time, and
within budget. Your reputation will become that of someone who gets the job done.

Testing and Calibration

Testing is a major part of quality. It is also an important consideration in design. A good design includes hardware and software self-test routines. An extra connector that brings out useful test points is a good idea. Software routines that were originally used for debugging the design can be reused to provide access to the programming. This can make troubleshooting much, much easier. Test and calibration notes placed on the PCB silkscreen are also very useful.

It used to be that numerous adjustments were needed for any piece of hardware. Each adjustment required measurements and time. Each adjustment could be mal-adjusted and was susceptible to tweaking by the user. Nowadays, this may no longer be necessary. Embedded microprocessors (µPs) are common and many include analog-to-digital converters (A/D). So, instead of calibrating out production variations, the µP can compensate for these variations.

If you aren’t doing this already, you should. It makes no sense to waste the capabilities of the µP and increase the production time for calibration and testing. Remember: A day or so spent during the design cycle can save a tremendous amount of production testing time. A 5 minute savings for 10,000 units is 833 hours of production labor — and that doesn’t include the savings from decreased troubleshooting, if needed.

ISO 9000

ISO 9000 (and its variations — 9001, etc.) has been around for about 10 years. It is an international standard for quality management. Note that it is NOT a standard for quality control. The basic premise of ISO 9000 is “if a quality assurance process is correctly established, then good quality should follow.” This is a commonly accepted idea. The US military has been using something similar for a long time. For the most part, this approach works (based on information from Quality Manager’s Complete Guide to ISO 9000 by Clements, 1993, Prentice Hall).

ISO 9000 can have many benefits for a company. This is especially true for firms that deal with the European Community. ISO 9000 provides a means of conferring credibility by indicating that the company meets an objective standard of quality management.

An interesting point is that ISO 9000 certification is performed by a third party, which is certified by a national body of accreditation. This is not the typical method. For example, if you need MIL-SPEC certification, you get it from the Department of Defense. Federal Communication Commission (FCC) compliance comes directly from the FCC.

With ISO 9000, you hire a “registrar” to assess your quality procedures. (The cost starts at about $10,000.00 and can go significantly higher.) However, the registrar does not require a specific set of tests or procedures. Rather, he or she will examine your documented tests and procedures to determine whether they are adequate, providing more flexibility.

We also see that ISO 9000 is a top-down approach. As noted above, it is a management system. This means that management must be involved. In particular, a quality management department (different from quality control) will have to be developed. Being a management department, upper management would also be involved. This is good, though. As we saw before, quality requires teamwork. The whole company should be involved in making quality products.

This tells us a number of things. If you already have a good system in place, reasonable management that encourages quality, and effective teamwork and communication between departments, then implementing ISO 9000 should be fairly straightforward. Obviously, if you don’t, then ISO 9000 — or any quality standard — will be difficult to accomplish.

Quality Through Rules

ISO 9000 has 20 “elements.” Each element requires a detailed
document that states how you manage that part of the quality process. These elements are: Management Responsibility, Quality System, Contract Review, Design Control, Document Control, Purchasing, Purchaser Supplied Product, Product Identification and Traceability, Process Control, Inspection and Testing, Inspection/Measuring and Test Equipment, Inspection and Test Status, Control of Nonconforming Product, Corrective Action, Handling, Storage, Packaging and Delivery, Quality Records, Internal Quality Audits, Training, Servicing, and Statistical Techniques. Not all of these elements are required for every business.

You can see that a lot of paperwork is involved. You create all the paperwork. Presumably, the departments that are affected by the sections will write those documents. The registrar verifies that the procedures in the documents meet the necessary standards and that you actually perform those procedures.

There are three levels of detail. The first documents, or Level I, are brief policy statements. Level II documents are the actual departmental procedures. Level III documents confirm that the Level II procedures are actually being followed (like test and calibration results). ISO 9000 is probably too involved for very small companies.

There is certainly a legitimate question here: Do rules create quality or just the appearance of quality? As we noted at the start, the attitude toward quality is important for everyone. A significant aspect of ISO 9000 is that management must make a serious commitment to quality. We also noted that management’s attitude is a critical factor in creating an atmosphere that fosters quality. Therefore, by forcing management to acknowledge and support the ISO 9000 standards, management is forced to provide the tools and materials necessary for quality design and production. This can certainly improve quality.

Of course, it is also possible to try to bypass the procedures after the registrar leaves. However, this is not easy to do. ISO 9000 is really a bureaucracy. It creates a paper trail that is difficult to conceal or falsify and there isn’t really much point in trying to do so. The registrar makes two unannounced visits each year to verify that all the procedures are being followed. Upper management takes a dim view of middle managers who put the company’s health at risk, especially since ISO 9000 certification can be a very important asset to a company.

Therefore, it is reasonable to believe that rules can improve quality. It doesn’t mean that the quality is the best that’s possible. Nor does it mean that all ISO 9000 certified companies provide the same quality. It does create and foster management’s commitment to quality and that’s certainly a very good thing.

ISO 9000 doesn’t guarantee that quality problems won’t arise. No set of rules can do that, but they do create a framework that can be used to address these problems. For example, it’s harder for a manager to declare a development schedule by whim. The ISO 9000 documents specify what needs to be done. These specifications have already been accepted by the manager. Therefore, the manager can be shown to be violating the ISO 9000 standards with his silly schedule. A more reasonable design timeline can result from using the ISO 9000 standards as a reference.

**Conclusion**

Quality is a team effort. It requires communication and coordination between departments, as well as a commitment by management. The attitude of every player is important. It only takes one person or one department to create significant quality problems. The ISO 9000 standard is a management tool that can be used to improve quality — perhaps significantly — by forcing management to take an active role in fostering and supporting a quality atmosphere throughout the company. **NV**
I'm trying to find service information or help for a BSR MCD8090 AM/FM Stereo Receiver. This unit was called a "Thunder Thrower" and was purchased from DAK Industries. The FM section is not working. Any help would be appreciated.

#2051 Mike Uschak
Loyalhanna, PA

I recently purchased a 48 VDC to 12 VDC switching power supply from a surplus place. What are the general rules of thumb for getting this thing to work? I know switchers need a load, but on which output? It has +3 V, +5 V, -12 V, and +12 V outputs. I am only interested in the +12 @10 A output. This supply has a couple of sensing circuits; what do they usually tie to? The supply house doesn't acknowledge any tech questions — they just sell the stuff. The factory made these on a special run and doesn't want to admit that they made the thing. Now, I'm out in left field trying to get it to work.

#2052 Bob Sheetz
Ocala, FL

I'm working on an old Epiphone Electar Zephyr guitar amp. It looks like it's from the 30s or 40s. I got the amp working, but I can not get the vibrato to work. The oscillator is very weak. It looks like someone worked on it before me and rewired the vibrato circuit. I cannot find a schematic for it. Does anyone have one or know how it is wired? The output of the oscillator goes to the grids of the two 6V6s.

#2053 Jon Garee
Newark, OH

I need to purchase a good, reliable, and low cost schematic capture/board layout program. Suggestions?

#2054 Aldo Powell
via Internet

I have a bunch of unmarked LEDs. Is there any way to determine the specs (forward voltage) of an LED if you don't already know it?

#2055 Jeff Rocchio
via Internet

How can I restrict outgoing calls on my land line from one phone?

#2056 Bill Gregory
via Internet

I am looking for a wiring diagram to help me build a cable tester. The cables have between six and 12 wires.

#2057 Nestor Quiroga
via Internet

What circuitry could I use to determine the winner of a Pine Box Derby race? These little cars cross the finish line at very fast speeds and are usually only milliseconds apart. I would like to use infrared or laser beams to be broken by the cars as the trigger for the circuit to determine the winner.

#2058 Bob Sheetz
Ocala, FL

ANSWERS

I got the new computer with Windows XP on it. (My old computer had Windows 98.) I use a...
DOS program to communicate with a PLC (programmable logic controller) through the serial port. The DOS program loads and works, but it will not communicate through the serial port. I’ve tried different settings and the Windows 98 compatibility mode. The program tries to access the PLC, but it times out. If I unplug the serial cable, it gives a communication error.

How do you get the XP serial port to work using older programs?

The manufacturer of the software does not have an answer, but they want to sell me new software that will run under XP — though they removed the features I use the most.

Windows XP behaves very differently from Windows 98 in three crucial ways:

1) Direct control of hardware, such as parallel and serial ports, is blocked! You need a driver called "directio.exe" to allow your program direct access to hardware. Get it at www.directio.com/index.htm or www.powerbasic.com/files/pub/tools/win32/.

2) You cannot boot to the MSDOS C> prompt, since XP is no longer built on MSDOS.

3) The DOS windows from "command.com" and "cmd.exe" are shells running on top of XP.

You could run a dual boot system if you ran the upgrade to XP from Win 98 and placed the system into a separate directory. This doesn’t seem like as good a solution as #1 above.

Barry Cole
Sunnyvale, CA

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Discontinued it. Are there any other manufacturiers with a similar IC or is there a way to program a microcontroller to serve the same purpose?

Tim Fitzstephens
Kalamazoo, MI

#1 There is a greeting card module that plays three Christmas tunes that goes by the part number SG14. Here is one link that sells it for under $5.00.

www.web-tronics.com/carmelchris.htm

Daryl Rictor
via Internet

#2 Yes, there is a microcontroller that can play tunes! It’s called the PICAXE. It’s a PIC controller with a bootstrap program downloaded to it and it uses a PBASIC language that is very similar to the BASIC Stamp. In the command language is a TUNE command that will play music.

PICAXE.com has a wealth of information on the processor and how to program it. You will also find over 500 tunes ready to download.

The chip is very versatile, with many commands only found on very expensive controllers. The chip number is PICAXE 08M and the cost is under $4.00. Believe it or not, I have purchased them on eBay. They are available in the states at phanderson.com

B. Ward
via Internet

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I would like to make a PC keyboard emulator where toggling a switch could emulate everything from an “A” keypress to a “Ctrl+Alt+Shift+A.” A schematic would be great, but even a nudge in the right direction is appreciated.

Frank Mozingo
via Internet

#1 There are several commercial options available. Here are a couple:

www.3tronics.com/keyboard_emulator_price.htm

www.vetra.com/312txt.html

If you want to "do it yourself," you can look at the link below. I designed a PC keyboard decoder that would use a microcontroller to read the scan codes from a PC keyboard and provide the ASCII output. You could reverse this process to generate scan codes from discrete switch closures.

www.softcom.net/users/darylr/io/pckbavr.html

Daryl Rictor
via Internet

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I have a test set for aligning my ham radio equipment. I have no trouble aligning receivers with this equipment, but — when I attach three frequency counters to the output — the readings go wild. When I connect them to older signal generators, the responses are as expected. Hooking the test set to my oscilloscope, I see that the signal generator is synthesized, not a pure sign wave, and is chock full of harmonics.

How can I filter the output sufficiently so a frequency counter can be properly used?

John Ciperano, K4EBC
via Internet

Harmonics from the generator should not bother the counter, but ringing of the connecting cable will. It is likely that the older generator put out a sine wave that is less prone to ringing. Try connecting a 50 ohm termination at the counter end of the cable (and use a 50 ohm cable). That should solve the problem.

Russell Kincaid
Milford, NH
NUTS & VOLTS

Tech Forum

[1058 - January 2005]

I’m using an LM3909 in a circuit to control flashing red and green lights on a model railroad. Is there a pin-for-pin replacement for it? If not, is there one that isn’t pin-for-pin?

R. Thompson
Richmond, MO

As you know, the National Semiconductor LM3909 LED pulser has been discontinued, but the NET876 is a direct replacement for the LM3909. The original devices can still be found, but they are getting a little pricey. Use the Froogle option in the Google search engine (www.google.com) to search for the LM3909.

There is a replacement option that utilizes discrete components to synthesize the pulser device. You can find the information at: http://home.cogeco.ca/~rpaisley4/LM3909.html

Ronald H. Schafer
Cuyahoga Falls OH

[9046 - September 2004]

What happens when an EXE file is run on a PC? I would like to know where the contents of an EXE file will be loaded and so on. Also, I am confused with partitions on the hard disk drive. I would like to know how the partitions (i.e., C, D, etc.) are represented on the disk.

You’ve asked a couple of very complex questions. Books have devoted entire chapters — usually it takes more than one chapter — to describe “exactly” what happens when MS-DOS (or Windows) loads an .EXE file.

Just for starters, “where” the contents will be loaded is not constant. Loading will begin at the first available memory location, whatever that happens to be (“whatever” depends on what else is running, the hardware configuration of the machine, and several other factors). In that available space, the system first constructs the program environment, takes chunks from the disk file, and places them into memory.

There are specifications in the disk file that describe how the system should place the data in memory (starting at the lowest available address, the highest available address, etc.), as well as directives that identify pieces of the data that must be modified to reflect where that chunk or other chunks actually end up. Most of the required gyrations can be determined from studying a detailed description of the "MS-DOS executable file format" specifications. The rest can be found in a description of the MS-DOS exec program function call.

Microsoft Press has some reasonably good books that cover both subjects. As for partitions on disk drives, that is also a messy subject — although not as messy as program loading. The very beginning of the disk contains some information in fixed places. The first sector of the first track of the first platter contains something called the ‘Master Boot Record’ or "MBR." Part of the MBR is a block of data that describes the physical characteristics of the entire disk — number of heads, number of cylinders, number of sectors-per-track, etc.

Another part — known as the fdisk table or partition table — allows one to divide the disk into as many as four logical sections or partitions. Each partition is described by where on the disk it begins (i.e., what cylinder, head, and sector) and the total number of sectors (consecutive/contiguous from the starting point) that are part of that partition. There is also a flag for each partition to indicate what kind of file-system (or other type of use) is specified for that partition.

DOS recognizes two kinds of partitions: primary partitions, which will have a file system created directly for them, and extended partitions, which have another layer of indirection involved. They start with an extended partition table, which is similar to the primary one, except that it has space for describing eight sections instead of just four. Those descriptions are relative to the beginning of the extended partition, not to the start of the disk. Then, you create the actual file systems on those partitions within a partition section.

Finally, when DOS starts up, it looks for that fixed location information on each physical drive that is attached to the system and assigns drive letters to each primary partition where it finds an appropriate file system. After that, it goes back and checks for any extended partitions and assigns drive letters to each partition in a partition that has an appropriate file system present. Finally, DOS loads any installable drivers (e.g., for CD-ROM, etc.) and assigns any required drive letters for those devices.

I haven’t even touched on how data or files are represented in the MS-DOS file system. That’s another whole book.

The bad news is that all the above is a superficial explanation of what actually goes on. When you get down to the actual gory details, things are a lot more complicated and complex.

Now, aren’t you sorry you asked?

Robert Bonomi
Evanston, IL

[10041 - October 2004]

I picked up a Zenith TV — model H2017Y — from a hotel that was remodeling. I can’t get the AV inputs to work; it looks like some programming or setup is required. I don’t have an owner’s manual and would appreciate any help.

You can call Zenith Data Systems at (800) 227-3360; they’ll have service and owner’s manuals. If the set needs to be repaired, go to Howard W. Sams, www.hwsams.com for a service manual.

James Stotler
Pleasant Hill, CA
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Adaptor Fits CSI Stations 1 & 2, and also CSI906

Item# CSI-TWZ-STATION $29.00

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SMD RE-WORK SYSTEM w/Vacuum Pick-up tool

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